

# Catalysis effect on the CO<sub>2</sub> methanation using MgH<sub>2</sub> as hydrogen portable medium

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The feasibility of the reduction of CO<sub>2</sub> to CH<sub>4</sub> employing MgH<sub>2</sub> in the presence and absence of cobalt as catalyst was investigated for the first time, exploring different non-independent reaction conditions such as the grade of microstructural refinement, the molar ratio MgH<sub>2</sub>:CO<sub>2</sub>, reaction time and temperature. For the un-catalyzed process a methane yield of 44.6% was obtained after 24 h of thermal treatment at 400 °C employing a molar ratio of 2:1, through a methanation mechanism that involves the direct reduction of CO<sub>2</sub> and the generation of CH<sub>4</sub> via C as an intermediary. For the MgH<sub>2</sub> catalyzed process a methane yield of 78% was achieved by heating at 350 °C for 48 h, being 4:1 the optimal molar ratio. The global mechanism responds to a Sabatier process favored by Co as an active catalyst, together with reversed water gas shift reaction followed by methanation of CO in presence of steam. On account of the fact that it was proved that the use of catalyst allows lowering the operational temperature without collapsing the methane yield, this research provides an interesting insight of a thermochemical method for CO<sub>2</sub> reduction to CH<sub>4</sub> employing a solid hydrogen storage medium as H<sub>2</sub> source.

## 1. INTRODUCTION

Since the industrial revolution, global economic growth has been sustained by low-cost energy production based on the exploitation of fossil resources, first coal and later natural gas and oil, as well as its derivatives. It is clear that the current energy system lacks sustainability as it faces problems of scarcity and dependence on hydrocarbons, non-renewable primary sources as well as unfriendly effects on the environment.<sup>1</sup> In fact, the global energy matrix based on the use of hydrocarbons has generated a strong environmental impact. The emission of greenhouse gases due to human activity, mainly carbon dioxide, has been responsible for the so-called climate change that includes not only global warming but also changes in rainfall, winds, in the cryosphere and level from sea. Greenhouse gases (GHG) emissions have risen at a rate of 1.5% per year in the last decade and reached a record high of 55.3 GtCO<sub>2</sub>e in 2018.<sup>2</sup> Fossil CO<sub>2</sub> emissions from energy use and industry, which dominates total GHG emissions, grew 2.0 per cent in 2018, reaching a record 37.5 GtCO<sub>2</sub> per year. Based on recent researches,

specialists on the field have concluded that by 2030, emissions would need to be 25% and 55% lower than in 2018 to put the world on the least-cost pathway to limiting global warming to below 2 °C and 1.5 °C, respectively.<sup>2</sup> The strong growth in energy demand due to industrialization, the increase in urban population and improvements in the quality of life, along with the progressive depletion of fossil resources faces the world to a scenario of energy deficit. The technologies related to the capture and storage (CCS) and transformation of CO<sub>2</sub> into value-added products are attractive both from an environmental and economic point of view as it implies its reuse and recovery as a raw material.<sup>3,4</sup> Through various thermal or catalytic processes, CO<sub>2</sub> can be employed to synthesize a wide range of chemicals (urea, salicylic acid, carbonates, carboxylates, carbamates, acrylates, etc.) or different fuels (methane, methanol, olefins, etc.).<sup>5-7</sup> CO<sub>2</sub> conversion constitutes a promising alternative to employ a contaminant as a building block for fuels.

The methanation process, also known as Sabatier reaction, was first presented in 1902. It involves the combination of hydrogen with carbon dioxide at elevated temperatures and pressures in the presence of a catalyst to produce methane and water.<sup>8</sup> Recently, in the search of strategies that allow the storage of the excess renewable energy produced during peak generation periods, the study of this reaction has renewed relevance.<sup>9-12</sup> In this regard, Power-to-gas technologies seek the transformation of surplus renewable energy into a grid compatible gas, which can be used in future peak demand periods. Although this concept today cannot be achieved in a cost-effective manner, it offers the prospect of large-scale recycling CO<sub>2</sub> emissions, in combination with the use of renewable energy to form methane.<sup>9</sup> For example, instead of storing green H<sub>2</sub> produced via water electrolysis for later use as an energy vector in different applications, this H<sub>2</sub> can react with CO<sub>2</sub> through the Sabatier process to create methane, which can then be used on demand to generate electricity overcoming low points of renewable energy production.<sup>10-15</sup> The main advantage is that methane is a widely used fuel that has a large distribution infrastructure in many countries and it can be injected into the existing gas network, avoiding the challenges related to hydrogen

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† Electronic Supplementary Information (ESI) available: Calculation procedure S1: Methane yield calculation procedure and numerical examples. Figure S1: Raman spectrum of MgH<sub>2</sub> after reaction with CO<sub>2</sub> (molar ratio of 2:1) at 400 °C for 24 h. Figure S2: XRPD pattern of as milled sample and after thermal treatment (350 °C, 24 h) under CO<sub>2</sub>. Figure S3: Solid-state FTIR profiles for the as milled MgH<sub>2</sub>-10%Co and after thermal treatment (400 °C, 5 and 24h) under CO<sub>2</sub>. Figure S4: Raman spectra of MgH<sub>2</sub>-10%Co after reaction with CO<sub>2</sub> considering different experimental conditions. Figure S5: XRPD pattern of the sample MgH<sub>2</sub>-10%wt Co with a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 4:1 (Co milled during the last 10 minutes). Figure S6: XRPD profile of the sample MgH<sub>2</sub>-10%wt Co at 350 °C with a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 2:1. Table S1: Gas-phase composition determined by gas chromatography analyses of the MgH<sub>2</sub>-10wt % Co sample at 300 °C. Figure S7: XRPD profile of the sample MgH<sub>2</sub>-10%wt Co at 300 °C with a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 4:1. Figure S8: Equilibrium composition (mol%) as a function of pressure at 450 °C for a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 4:1 (A) and 2:1 (B). Figure S9: Equilibrium composition (mol %) as a function of temperature at 1 bar for molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 2:1. See DOI: 10.1039/x0xx00000x

storage. Through this strategy, renewable electric energy can be transformed into storable methane and CO<sub>2</sub> can be considered as an energy carrier for this process. In order to reach acceptable rate and selectivity for the methanation process, the use of appropriate catalysts is mandatory.<sup>16-18</sup> In fact, the lack of efficient and long-term operation catalysts limits its application in industrial scale.<sup>18</sup> This exothermic reaction ( $\Delta H^{298K} = -165 \text{ kJmol}^{-1}$ ) typically operates between 200 and 450 °C, depending on the catalyst and the experimental conditions (Reaction 1).<sup>19,20</sup> No general consensus exists on the reaction's operating mechanism, mainly due to the uncertainty in determining the intermediate compound involved in the rate determining step. The discrepancy lies in the fact of considering the CO as an intermediary or not.<sup>16</sup>

$\text{CO}_2(\text{g}) + 4\text{H}_2(\text{g}) \rightarrow \text{CH}_4(\text{g}) + 2\text{H}_2\text{O}(\text{g})$  ( $\Delta G^{298K} = -110 \text{ kJmol}^{-1}$ ) Reaction 1

Despite CO<sub>2</sub> methanation can be catalyzed by noble metals with high performance, the interest from an industrial view is limited due to their high costs and, instead, transition metals have been widely studied.<sup>16</sup> DFT calculations show spontaneous chemisorption of CO<sub>2</sub> on iron, cobalt, nickel and copper surfaces. It was demonstrated that the metal nature and its surface structure have a crucial role on the CO<sub>2</sub> chemisorption, affecting both the activation and the reduction steps involved in CO<sub>2</sub> hydrogenation.<sup>17</sup> Moreover, preservation and improvement of the metal activity can be achieved by selecting an appropriate support as they influence the activity, productivity and lifetime of the active phase.<sup>16</sup> The most usual supports are oxides (Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, ZrO<sub>2</sub>, TiO<sub>2</sub>, CeO<sub>2</sub>), zeolites, clays and mesoporous materials. The combination of the non-noble metal (one or several) with different supports, opens a range of catalyst behaviors due to the beneficial effects (or not) of the metal-support interaction.<sup>18,21-28</sup>

The reaction between hydrogen storage alloys with CO<sub>2</sub> was first explored in 1990. The oxidized surfaces allowed the generation of new carbonate species.<sup>29,30</sup> More recent studies showed that CO<sub>2</sub> can be reduced on the surface of hydrides that act as catalysts, by means of the Sabatier reaction allowing the conversion of CO<sub>2</sub> to methane and closing the cycle of carbon.<sup>31-37</sup> This allows the use of H<sub>2</sub> stored safely in a solid matrix (MH<sub>x</sub>, M: metal, H: hydrogen), which could act as a catalyst for the transformation of CO<sub>2</sub> into a gaseous fuel. In particular, it was found that some complex hydrides such as, for example, Mg<sub>2</sub>NiH<sub>4</sub>, Mg(BH<sub>4</sub>)<sub>2</sub>, and LiAlH<sub>4</sub> possess good catalytic properties for the hydrogenation of CO<sub>2</sub>, generating different chemical compounds of industrial interest.<sup>31-35</sup> Although the decomposition of alanates in atmospheres with CO<sub>2</sub> has been little explored, it is known that at temperatures greater than 120 °C, LiAlH<sub>4</sub> reacts with CO<sub>2</sub>, producing CH<sub>4</sub>, H<sub>2</sub> and metal oxides.<sup>32</sup> Regarding borohydrides, the open structure of the gamma-Mg(BH<sub>4</sub>)<sub>2</sub> phase and the high Mg<sup>2+</sup> concentration make it an ideal material to be considered for CO<sub>2</sub> conversion, which occurs rapidly at low temperatures.<sup>33</sup> Through the study of the catalytic interactions of the surface of Mg<sub>2</sub>NiH<sub>4</sub> with CO<sub>2</sub> during dehydrogenation, it was postulated that the dissociation of H<sub>2</sub> molecules on the surface is not the limiting step but adsorption dissociative of CO<sub>2</sub> molecules on the surface of the hydride.<sup>31</sup> The authors reported the formation of CH<sub>4</sub> and H<sub>2</sub>O at 330 °C in the first cycle and, due to the formation of Ni nanoparticles that increase the catalytic activity of the system, it decreased to 280 °C in subsequent cycles.<sup>31</sup> Recently, the complex hydrides Mg<sub>2</sub>FeH<sub>6</sub> and

Mg<sub>2</sub>NiH<sub>4</sub>, prepared by a two-step procedure involving milling and sintering at high temperature, were proved to be good dual conversion promoters and hydrogen sources for the selective CO<sub>2</sub> conversion to CH<sub>4</sub>. It was revealed that the reversed water-gas shift reaction (WGS) followed by the methanation of CO in the presence of steam dominates the process for the Mg<sub>2</sub>FeH<sub>6</sub>-CO<sub>2</sub> system, whereas for the Mg<sub>2</sub>NiH<sub>4</sub>-CO<sub>2</sub> system, the CO<sub>2</sub> direct reduction has a strong contribution.<sup>34</sup> Interestingly, it was proved that the synthesis method of Ni metal complex hydride has an impact on the global mechanism. Under the same experimental conditions, the methanation via as-milled Mg<sub>2</sub>NiH<sub>4</sub> was proved to be faster and different from the one via as-sintered Mg<sub>2</sub>NiH<sub>4</sub>, with the presence of graphite in the solid phase.<sup>35</sup> In addition, recently, the thermochemical CO<sub>2</sub> reduction by alkali metal hydrides (LiH and NaH)<sup>34</sup> or alkaline-earth metal hydrides (CaH<sub>2</sub> and MgH<sub>2</sub>)<sup>35</sup> in the absence of catalyst was presented. Both investigations agree that the yield of methane obtained depends strongly on the type of hydride, the H<sub>2</sub>:CO<sub>2</sub> molar ratio and reaction conditions (temperature and time). The best performances were achieved by heat treatment at 450 °C for 48 h.<sup>36,37</sup> In that condition, methane yields were calculated to be 54.2, 68.0, 80.1 and 88.0 % employing NaH<sup>36</sup>, MgH<sub>2</sub><sup>37</sup>, LiH<sup>36</sup> and CaH<sub>2</sub><sup>37</sup>, respectively.

In this work, for the first time the reduction of CO<sub>2</sub> to CH<sub>4</sub> using a hydride in the presence and absence of catalyst was investigated, allowing the study of different variables such as the microstructure, pressure, molar ratio H<sub>2</sub>:CO<sub>2</sub>, temperature and reaction times under the same conditions and using the same experimental set-up for the comparison between the un-catalyzed and catalyzed processes. Owing to the fact that our investigation group have previously explored the methane production *via* a catalytic process promoted by hydrides containing iron and nickel<sup>34,35</sup>, in this work the use of cobalt was considered as this transition metal was also proved to have an excellent catalytic activity.<sup>16,17,38</sup> In particular, the feasibility of the use of MgH<sub>2</sub> for CO<sub>2</sub> conversion to CH<sub>4</sub>, analyzing the role of cobalt as catalyst was investigated deeply and the reaction conditions that favor the desired products were explored. For the MgH<sub>2</sub> catalyzed process a methane yield of 78% was obtained by heat treatment at 350 °C for 48 h. This yield is not only considerably higher than the one previously reported at 350 °C (17 %) but, interestingly, it is also higher than that reported at 450 °C (68%).<sup>37</sup> Then, this research provides an interesting thermochemical method for CO<sub>2</sub> methanation employing a widely studied solid hydrogen storage medium (MgH<sub>2</sub>) as H<sub>2</sub> source at lower temperatures.

## 2. EXPERIMENTAL

### 2.1 Materials preparation

The starting materials were commercial MgH<sub>2</sub> (Aldrich, 98%) and metallic Co (Aldrich, 99.9%). Due to the high reactivity of the samples, they were handled in a MBraunUnilab argon-filled glove box, with oxygen and moisture levels lower than 10 ppm. For all studies, high purity argon (Linde, 99.999%) was used. Two samples were prepared by mechanical milling (MM) in order to reduce particle size and achieve homogenous mixing: I) MgH<sub>2</sub> and II) MgH<sub>2</sub>-10 wt% Co, using a sequence of 15 min milling and 10 min pause in

a planetary ball mill (Fritsch Pulverisette 6). Samples were ball milled during 5 h at 500 rpm with a ball to powder mass ratio of 53:1.

## 2.2 Characterization of the samples

The reaction between the samples and CO<sub>2</sub> was studied under flow and static conditions.

The dynamic measurements were performed in a TGA analyzer (TG-HP50, TA Instruments). In these experiments, the samples were heated at 5 °C.min<sup>-1</sup> up to 400 °C in a continuous flow of CO<sub>2</sub>. Additionally, the experiment was done using a flow of He to analyze the decomposition of the sample in an inert atmosphere.

A stainless steel reactor coupled to a Sieverts volumetric equipment that allows the selection of the pressure and temperature was employed to study the reactivity under static conditions. A specific mass of each sample was introduced in the reactor inside the glove box to avoid contamination with oxygen or air humidity and then heated up with a ramp of 10 C.min<sup>-1</sup> to different temperatures (300, 350 and 400°C) under CO<sub>2</sub> pressure. Two different molar ratios MgH<sub>2</sub>:CO<sub>2</sub> were considered (4:1 or 2:1). The selected ratio, temperature and length of the thermal treatment are indicated in each experiment. The hydride amount was estimated taking into account the theoretical MgH<sub>2</sub> hydrogen storage capacity.

The composition of the gases after thermal treatment under CO<sub>2</sub> was studied employing gas-phase FTIR analyses (FTIR, Perkin Elmer Spectrum 400 with MCT detector) and gas chromatography (GC, Agilent Technologies GC System 7820A). For GC experiments 1 ml of the released gas was taken using a syringe, which was injected into the GC equipment. The molar amounts of gaseous CO<sub>2</sub>, CH<sub>4</sub> and CO were quantified using calibration curves. Methane yield was calculated as: the ratio between the produced CH<sub>4</sub> moles and the total CO<sub>2</sub> moles at the beginning of the reaction (a numerical example is available at Supplementary Material). For IR spectroscopy measurements, the gases released were collected in a degassed quartz optical cell with KBr windows. The gas phase spectra at room temperature were taken with a resolution of 0.5 cm<sup>-1</sup>.

The structural and thermal properties of the as-milled and after thermal treatment under CO<sub>2</sub> solid samples were studied using X-ray powder diffraction (XRPD, DRX Bruker D8 Advance), Fourier transform infrared spectroscopy (FTIR, Perkin Elmer Spectrum 400 with MCT detector) and Raman spectroscopy (LabRAM HR Evolution Raman microscopy). During the XRPD data collection, all the samples were kept under an Ar atmosphere using an airtight holder, which has a bump in the zone of 2θ=15-25°, to prevent any reaction between samples and air. For IR spectroscopy measurements, the samples were ground with dry KBr under a purified argon atmosphere, pressed to pellets and placed in a specially designed airtight cell. Handling was done inside the glove box to avoid contact with air. Solid state IR spectra were obtained in the range of 4000–800 cm<sup>-1</sup> with a resolution of 4 cm<sup>-1</sup>. Raman spectroscopy was employed to analyze the solid samples after treatment under CO<sub>2</sub> in order to identify carbon and carbon compounds at room temperature and using a laser wavelength of 514 nm. Morphological and agglomerate size distribution analyses of the samples were performed by Scanning electron microscopy (SEM, SEM-FIB, Zeiss, Crossbeam 340), employing dispersed

powders a carbon tape. Elemental analyses of the materials were also performed by energy-dispersive X-ray spectroscopy (EDXS) on SEM.

## 2.3 Thermodynamic calculations

The equilibrium compositions for the MgH<sub>2</sub>-CO<sub>2</sub> system as a function of the temperature and also as a function of pressure were calculated using HSC Chemistry Windows.<sup>39</sup> Given all the species (reactants and products) in a reaction system, the software determines the distribution of the products where the Gibbs free energy of the system reaches its minimum. The calculation was conducted based on gas phase containing CO<sub>2</sub>, H<sub>2</sub>, CO, CH<sub>4</sub>, H<sub>2</sub>O, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>6</sub> and CH<sub>3</sub>OH and solid phase containing Mg, MgO, Mg(OH)<sub>2</sub>, MgCO<sub>3</sub>, MgC<sub>2</sub>, Mg<sub>2</sub>C<sub>3</sub> and C.

## 3. RESULTS

### 3.1 CO<sub>2</sub> conversion in the presence of MgH<sub>2</sub> without catalyst.

To investigate the conversion of CO<sub>2</sub> in the presence of MgH<sub>2</sub> without any catalyst addition, the as-milled hydride was heated up to 400°C in static conditions under a CO<sub>2</sub> atmosphere during 24 h. Two different molar ratios MgH<sub>2</sub>:CO<sub>2</sub> were considered (4:1 and 2:1) in order to evaluate its influence on the product formed and further elucidate the reaction mechanism. Ball milling was employed to activate the commercial MgH<sub>2</sub>, as it is expected that its reactivity increases with microstructure refinement. This effect can be associated to both the agglomerate size reduction and the crystallite size reduction. The bigger exposed area available for the reaction is responsible for the increase in reactivity.

The evolution of the phases due to the interaction with CO<sub>2</sub> was studied by XRPD and FTIR (Fig. 1). Although the XRPD profile of the as-milled MgH<sub>2</sub> reveals a low crystallinity after milling, the absence of impurities was confirmed (Fig. 1A). The broad and weak diffraction peaks show that mechanical milling was effective in reducing strongly the particle size. After thermal treatment under CO<sub>2</sub>, for both, the 4:1 and the 2:1 samples, Mg and MgO were easily detected. The main difference is that, for the former, unreacted MgH<sub>2</sub> was identified. In addition, solid-state FTIR revealed that for the 4:1 sample no carbonate phases were formed and the presence of unreacted MgH<sub>2</sub> cannot be discarded (Fig. 1B). On the other hand, for the 2:1 sample no MgH<sub>2</sub> was detected, whereas some bands at the band region 1600–600 cm<sup>-1</sup> could be related to the presence of carbonates favored by the higher CO<sub>2</sub> pressure.<sup>40,41</sup> Among them, the bands located at 1063, 879 and 1415 cm<sup>-1</sup> could be attributed to the vibration modes (ν<sub>1</sub>, ν<sub>2</sub> and ν<sub>3</sub>, respectively) of superficial carbonate species on MgO.<sup>40</sup> For MgH<sub>2</sub>, stretching bands consists in various peaks with the strongest one at 1246 cm<sup>-1</sup> and the bending band at 658 cm<sup>-1</sup>.<sup>42</sup>

The presence of elemental C (bands G and D) and carbonates was confirmed by Raman measurements (see Fig. S1).

As shown in the SEM images (Fig. 2), the morphological characteristic of the as-milled MgH<sub>2</sub> agglomerates is its spongy form and its wide size agglomerate distribution between 5 and 50 microns.

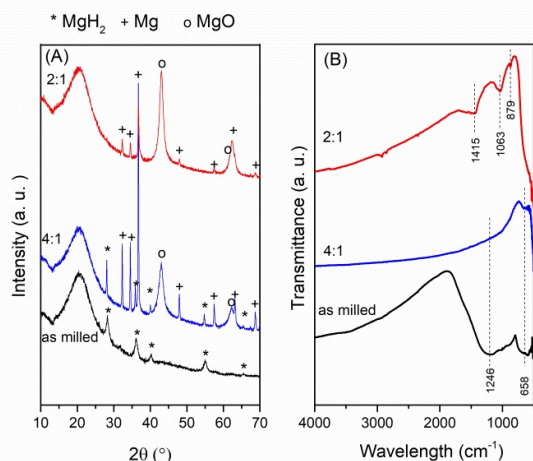


Figure 1: XRPD patterns (A) and solid-state FTIR spectra (B) of as-milled sample and after thermal treatment (400°C, 24 h) under CO<sub>2</sub>.

After thermal treatment under CO<sub>2</sub>, the sample is composed of micrometric agglomerates with appreciable amount of pores.

The average agglomerate size increased by treatment at 400 °C. Previous studies<sup>34</sup> in similar materials have revealed that the spherical particles correspond to MgO formed due to the CO<sub>2</sub> reduction in presence of MgH<sub>2</sub> (some of them are indicated in Fig 2D). Regarding the surface morphology, before the reaction, particles with straight edges were detected, while after the reaction all the particles are small and rounded, with round MgO particles.

The gas-state products of the reaction between MgH<sub>2</sub> and CO<sub>2</sub> were identified and quantified by gas chromatography. Clear H<sub>2</sub> and CH<sub>4</sub> chromatography's peaks were observed. An excess of CO<sub>2</sub> and co-generation of minor percent of CO were also detected in some cases (see Table 1).

Increasing the CO<sub>2</sub> proportion elevates the mole percentage of CH<sub>4</sub> from 17.8 (relation 4:1) up to 46.4 (relation 2:1) after 24 h at 400°C.

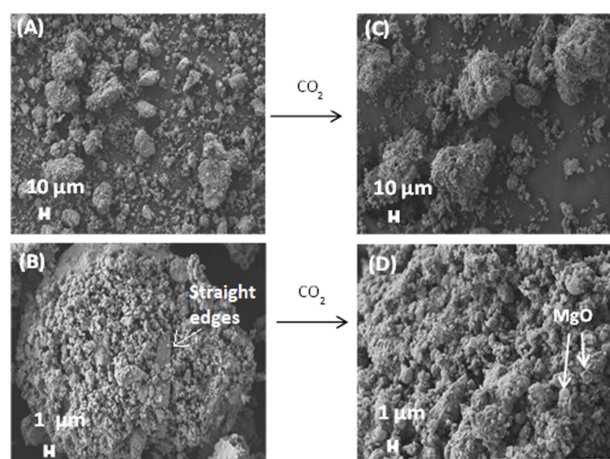


Figure 2: SEM images of the as-milled MgH<sub>2</sub> (A, B) and after thermal treatment under CO<sub>2</sub> (C, D).

Moreover FTIR analyses of the resulting gas phase after reaction with CO<sub>2</sub> at 400°C, considering a molar ratio of 2:1, were performed to prove the presence or absence of H<sub>2</sub>O. In Figure 3 the patterns for 5 and 24 h are compared. Although GC experiments revealed the presence of a small amount of CO<sub>2</sub> and CO after 24 h (see Table 1), these species are not detected by this technique as the quantity is below the detection limit. As expected, when reaction time was increased, CO<sub>2</sub> is consumed and the bands corresponding to CO are no longer identified. The presence of H<sub>2</sub>O is not unequivocally established. The presence of higher hydrocarbons such as ethane or propane (C<sub>x</sub>H<sub>y</sub>) is suspected due to the weak absorption peaks at 1470 and 2968 cm<sup>-1</sup>.<sup>36,43</sup>

In order to analyze the role of temperature, the sample was thermal treated under CO<sub>2</sub> (with a relation MgH<sub>2</sub>:CO<sub>2</sub> of 2:1) at a lower temperature: 350°C instead of 400°C. The reaction yield drops drastically from 44.9% at 400°C to 0.4% at 350°C (see Table 1). XRPD analysis shows that the solid sample is mainly composed of unreacted MgH<sub>2</sub>, whereas Mg and MgO can also be identified (see Fig S2). Although MgH<sub>2</sub> can be decomposed under certain backpressure of an inert gas at temperatures lower than 400°C, this observation indicates that the presence of CO<sub>2</sub> inhibits its decomposition. For the set of experiments performed, the best results were obtained for a thermal treatment of 24 h at 400°C considering a ratio MgH<sub>2</sub>:CO<sub>2</sub> of 2:1. As show in Fig. 1, for this sample no MgH<sub>2</sub> remains in the solid product, which means that the experimental conditions allowed the complete decomposition of the reactant.

### 3.2 CO<sub>2</sub> conversion in the presence of MgH<sub>2</sub> with Cobalt as catalyst.

#### 3.2.1. Characterization of the as-milled sample

The as-milled doped sample MgH<sub>2</sub>-10wt%Co was analyzed by XRPD (Fig. 4). As expected, it is composed of MgH<sub>2</sub> and metallic Co (2θ= 41.7, 44.8, 47.6°) and no other Co-containing compounds were formed due to mechanical milling. SEM images of the sample after ball milling showed that the average agglomerate size was not modified by the presence of Co (~ 40 μm) and the element mapping obtained by EDXS indicates homogeneous distribution of Co (Fig. 5).

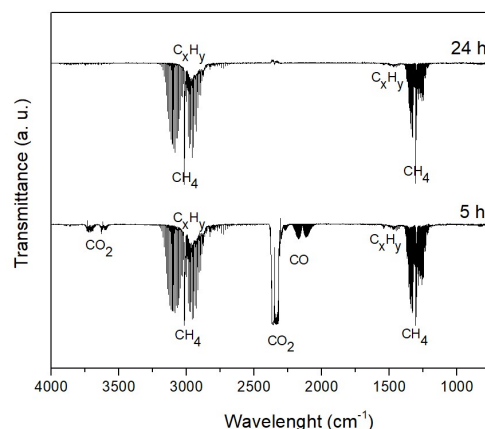


Figure 3: Gas-state FTIR patterns for the as-milled sample after thermal treatment under CO<sub>2</sub> (2:1) at 400 °C for 5 h (as-reacted) and 24 h (after dilution).

Table 1: Gas-phase composition determined by gas chromatography analyses for as-milled MgH<sub>2</sub>.

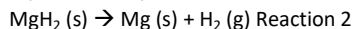
Temperature (°C)	MgH <sub>2</sub> :CO <sub>2</sub>	Reaction time (h)	Molar percentage of CH <sub>4</sub> (%)	Molar percentage of CO <sub>2</sub> (%)	Molar percentage of CO (%)	Molar percentage of H <sub>2</sub> (%)	CH <sub>4</sub> yield (%)
400	4:1	24 h	17.8	0.6	0	81.6	42.4
400	2:1	5 h	6.8	37.9	6.8	48.5	4.3
400	2:1	24 h	46.4	0.9	<1000 ppm	52.7	44.6
350	2:1	24h	3.8	67.5	5.2	23.5	0.3

### 3.2.2 Reactivity of MgH<sub>2</sub> with CO<sub>2</sub> under dynamic conditions

The carbon dioxide absorption of MgH<sub>2</sub> and MgH<sub>2</sub>-10wt% Co after ball milling for 5 h was first studied and compared under dynamic conditions by thermogravimetry (Fig.6).

Dehydrogenation temperature of the as-milled samples was analyzed using TG in He flow with a heating ramp of 5°C/min. The decomposition reaction of the doped and un-doped MgH<sub>2</sub> displayed a one-step dehydrogenation process with a big difference on the temperature at which decomposition begins. TG measurements revealed that the dehydrogenation temperature of MgH<sub>2</sub> (330°C) was lowered ~80°C by the addition of Co (estimated at 0.1% of mass change).

Regarding the hydrogen content, at 400°C MgH<sub>2</sub> released 7.3 wt% H<sub>2</sub>, which represents the 96% of its theoretical capacity (7.6 wt% H<sub>2</sub>). Hence, the decomposition of MgH<sub>2</sub> under inert gas flow can be represented by Reaction 2.



As expected, the addition of Co induced a drop in the hydrogen capacity. 6.2 wt% H<sub>2</sub> was released, whereas the expected theoretical value considering the amount of dopant is 6.8 wt% H<sub>2</sub>.

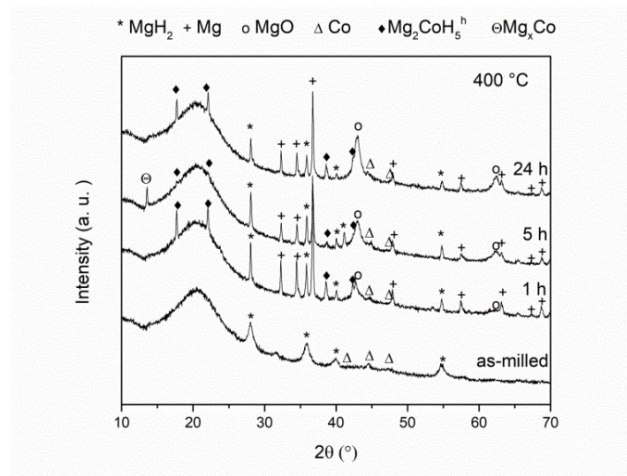


Figure 4: XRPD patterns of the as-milled and after thermal treatment under CO<sub>2</sub> at 400°C of the MgH<sub>2</sub>-10wt% Co sample.

On the other hand, thermogravimetric results show that when both samples are exposed to a CO<sub>2</sub> flux from room temperature up to 400 °C, mainly mass gain is observed (Fig. 6).

The weight increase does not change considerably when Co is incorporated by ball milling. In fact mass change is of about 12% in both cases, with a slight mass loss near 400 °C.

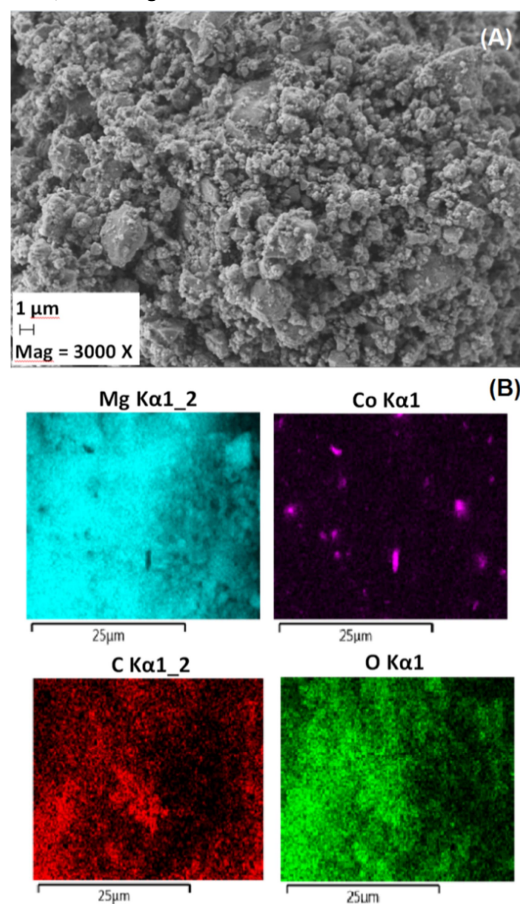


Figure 5: (A) SEM images of secondary electron; (B) Elemental mapping of the as-milled MgH<sub>2</sub>-10wt% Co sample.

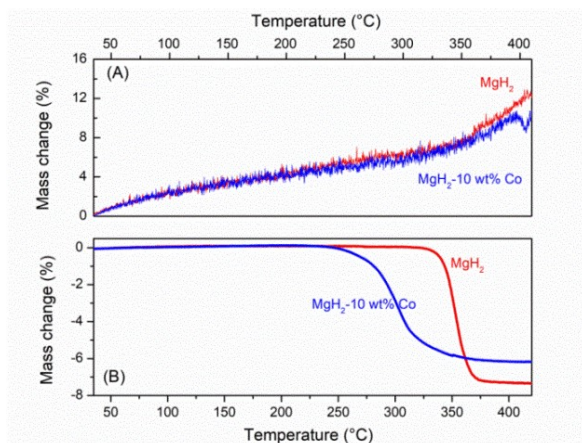


Figure 6: Thermogravimetric measurements of the MgH<sub>2</sub> and MgH<sub>2</sub>-10wt%Co samples under CO<sub>2</sub> (A) and He (B).

It has been already demonstrated that for certain hydrides studied, the initial CO<sub>2</sub> absorption induces only mass gain and retard the dehydrogenation by passivation or oxidation of the hydride surface.<sup>31,34</sup> This means H<sub>2</sub> is released at higher temperatures when the hydride is exposed to a CO<sub>2</sub> flux respect to an inert gas flow.

### 3.2.3 Reactivity of catalyzed MgH<sub>2</sub> with CO<sub>2</sub> under Static conditions

To investigate the conversion of CO<sub>2</sub> in the presence of catalyzed MgH<sub>2</sub> after milling by heating in static conditions, different temperatures and durations of thermal treatment were employed. Unless otherwise stated, in all cases MgH<sub>2</sub>:CO<sub>2</sub> ratio of 4:1 was considered.

GC analyses were performed to analyze the gas phase obtained after reaction at 400°C, varying the duration of the thermal treatment: 1, 5 and 24 h. It was observed that when reaction time was increased, the gas phase was richer in CH<sub>4</sub> and poorer in CO<sub>2</sub> and CO (see Table 2). Notably, for 24 h a CH<sub>4</sub> yield of 60.9 % was reached.

The obtained solid products after thermal treatment under CO<sub>2</sub> were analyzed by XRPD (see Fig. 4). In the three XRPD patterns Mg, MgO and MgH<sub>2</sub> are easily identified. Moreover, the presence of small peaks corresponding to metallic Co cannot be discarded. Interestingly after 1 h of thermal treatment the complex mixed Co and Mg hydride with hexagonal structure (Mg<sub>2</sub>CoH<sub>5</sub><sup>h</sup>) was formed and after 24 h it was still detected. However, at an intermediate time, Mg<sub>2</sub>CoH<sub>5</sub> is hardly observed but an intermetallic compound, identified by its most intense peak at 2θ=13.4°, which corresponds to Mg<sub>x</sub>Co was identified.<sup>44</sup> In literature there are two different reported processes through which this intermetallic compound can be formed: 1) Diffusion in solid state of Mg and Co powders during thermal treatment or 2) Hydrides (Mg<sub>2</sub>CoH<sub>5</sub> or Mg<sub>6</sub>Co<sub>2</sub>H<sub>11</sub>) decomposition. When MgCo is exposed to heat treatment in the presence of H<sub>2</sub> and free Mg, Mg<sub>2</sub>CoH<sub>5</sub> can be formed according to: MgCo(s) + Mg(s) + 5/2H<sub>2</sub>(g) → Mg<sub>2</sub>CoH<sub>5</sub>(s).<sup>45</sup> Then, the coexistence of metallic Co and a co-formed phase such as Mg<sub>2</sub>CoH<sub>5</sub> or Mg<sub>x</sub>Co may have a catalytic role.<sup>45</sup> Solid-state FTIR analyses proved the presence of carbonate species by the identification of two bands

located at 1063 and 1260 cm<sup>-1</sup> which correspond to carbonate unidentate and bidentate, respectively, on MgO (see Fig. S3).<sup>40,41</sup> Raman measurements of the obtained solid samples allowed discarding the presence of elemental C (see Fig. S4).

Seeking to disfavor the formation of Co-containing compounds in order to have available metallic cobalt, a new sample in which the Co was incorporated to the MgH<sub>2</sub> at the end of the ball milling (during the last 10 minutes) was prepared. As an unexpected result, after thermal treatment under CO<sub>2</sub> for 5 h (denoted in Table 2 as 5h\*), similar results were obtained. The complex hydride is not formed, metallic Co is identified and the peak corresponding to the intermetallic is incipient, which means that even in this case Co reacts to form Mg<sub>x</sub>Co (see Fig S5). Thus, the addition of Co at the end of the milling processing did not have a major effect on the CH<sub>4</sub> yield. Considering the set of experiments presented in Table 2, unlike what was observed for the sample without catalyst, there are no major differences when increasing the heat treatment time from 5 to 24 hours at 400°C. For the 24h-treated sample, in addition to CH<sub>4</sub>, the presence of H<sub>2</sub>O was confirmed by gas-phase FTIR and CO<sub>2</sub> and CO were not detected as the quantity is below the detection limit (see Fig. 7). Moreover, the presence of superior hydrocarbons is discarded.

SEM images of the sample after 5 h of thermal treatment under CO<sub>2</sub> showed the existence of micrometric agglomerates with a great amount of pores (Fig. 8). The element mapping obtained by EDXS shows a homogenous distribution of Co. Although some rounded particles (MgO) were identified, the amount is lower than the observed for the sample without additive.

The viability of the CO<sub>2</sub> hydrogenation was analyzed at 350°C. At this temperature the reaction length was crucial. Unlike what was conditions, the gas phase was mainly composed of CH<sub>4</sub> (49.7 mol%) and H<sub>2</sub>, with a little excess of CO<sub>2</sub> (0.5mol%) and reaction yield increase up to 78%.

XRPD measurements obtained after CO<sub>2</sub> conversion at 350 °C (Fig. 9) showed that as the reaction time increases, the amount of MgH<sub>2</sub> decreases markedly, while the amount of Mg and MgO increases. At this temperature, after 5 h only the tetragonal phase of Mg<sub>2</sub>CoH<sub>5</sub> was detected (Mg<sub>2</sub>CoH<sub>5</sub><sup>t</sup>). At higher reaction times there is a structural phase transition, the tetragonal phase was hardly visible but the peaks corresponding to hexagonal Mg<sub>2</sub>CoH<sub>5</sub> appeared.

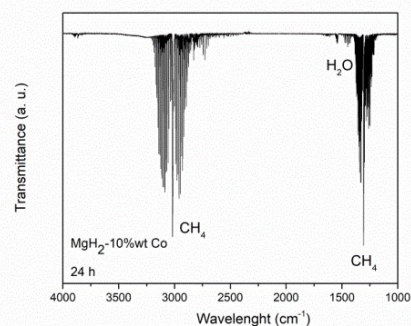
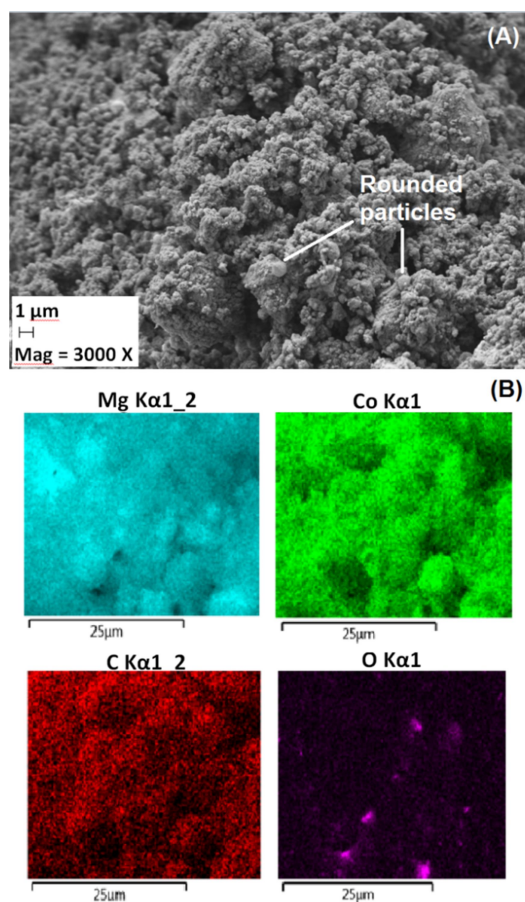


Figure 7: Gas-phase FTIR profile for the MgH<sub>2</sub>-10wt%Co after thermal treatment (400°C, 24h) under CO<sub>2</sub>.

Table 2: Gas-phase composition determined by gas chromatography analyses of the  $\text{MgH}_2$ -10wt %Co sample at 400°C.

Reaction time (h)	Molar percentage of $\text{CH}_4$ (%)	Molar percentage of $\text{CO}_2$ (%)	Molar percentage of CO (%)	Molar percentage of $\text{H}_2$ (%)	$\text{CH}_4$ yield (%)
1	6.3	21.8	0.1	71.8	15
5	34.2	7.7	0.2	57.9	57.1
5 *	32	9	0.1	58.9	61.3
24	38.2	0.8	<1000 ppm	61	60.9

Figure 8: (A) SEM images of secondary electron; (B) Elemental mapping of the  $\text{MgH}_2$ -10wt%Co sample after thermal treatment (400°C, 5 h) under  $\text{CO}_2$ .

Moreover the experiment was repeated considering a molar ratio  $\text{MgH}_2$ : $\text{CO}_2$  of 2:1 instead of 4:1 (24 h at 350 °C). Although the percentage of methane grew, a big amount of  $\text{CO}_2$  remained unreacted and CO was generated (see Table 3). This was reflected in the calculated methane yield (27.6%). The XRPD analyses of the solid product (Fig. S6) revealed the presence of unreacted  $\text{MgH}_2$ , as well as  $\text{MgO}$ ,  $\text{Mg}_2\text{CoH}_5$  (tetragonal and hexagonal phases) and metallic Co. Metallic Mg was hardly observed, which indicates that the majority was oxidized.

Motivated by the good results at 350°C, reaction temperature was further decreased to 300°C. However poor results were obtained ( $\text{CH}_4$  yield <1%) (see Table S1). Most of the  $\text{CO}_2$  remained unreacted and CO was considerably generated. Consistently, the XRPD pattern of the obtained solid sample showed a big amount of unreacted  $\text{MgH}_2$ . Mg was identified but no  $\text{MgO}$  was detected. Metallic Co is clearly identified and there are incipient peaks related to tetragonal  $\text{Mg}_2\text{CoH}_5$  (see Fig. S7).

\*  $\text{MgH}_2$  + Mg ○  $\text{MgO}$  △ Co ◆  $\text{Mg}_2\text{CoH}_5^h$  ■  $\text{Mg}_2\text{CoH}_5^t$  ⊖  $\text{Mg}_x\text{Co}$

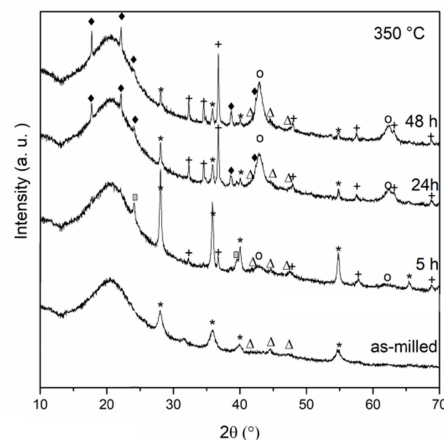
Figure 9: XRPD profiles of the as-milled  $\text{MgH}_2$ -10wt% Co sample and after thermal treatment at 350°C under  $\text{CO}_2$ .

Table 3: Gas-phase composition determined by gas chromatography analyses of the MgH<sub>2</sub>-10wt%Co sample at 350°C

MgH <sub>2</sub> :CO <sub>2</sub>	Reaction time (h)	Molar percentage of CH <sub>4</sub> (%)	Molar percentage of CO <sub>2</sub> (%)	Molar percentage of CO (%)	Molar percentage of H <sub>2</sub> (%)	CH <sub>4</sub> yield (%)
4:1	5	3.1	62.9	18.6	15.4	3.4
	24	42.3	0.6	<1000 ppm	57.1	59.7
	48	49.7	0.5	-	49.8	78
2:1	24	50.2	35	13	1.8	27.6

#### 4. DISCUSSION

The methanation mechanism is a complex process which depends on several factors: on the one hand it depends on the presence of catalyst and its nature and on the other, on the grade of microstructural refinement (in this case, provided by mechanical activation), reaction temperature and time. The calculated methane yields are represented in Figure 10. Moreover, Figure 11 displays a summary of the GC results, showing the molar fractions of both the CO<sub>2</sub> remained in excess and the generated CH<sub>4</sub> after thermal treatment in different operational conditions.

From figure 10, it can be observed that without catalyst a methane yield of 44.6% can be obtained after 24 h of thermal treatment at 400°C employing a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 2:1. In this condition, the gas phase is composed of 46.4 % of CH<sub>4</sub> with an excess of CO<sub>2</sub> of 0.9 % and a small amount of generated CO (<1000 ppm) (see Fig. 10). The presence of a small amount of superior hydrocarbons (ethane or propane) was proved by gas state FTIR (see Fig. 3). The solid product was demonstrated to be composed of Mg and MgO and no MgH<sub>2</sub> remained unreacted. Carbonate species were detected by solid state-FTIR (see Fig. 1B). Moreover the presence of C and carbonates was confirmed by FTIR and Raman measurements (see Fig. 1 and S1). When either the temperature or the reaction time is lowered, the performance values drop sharply and, logically, it is accompanied by a decrease in the amount of CH<sub>4</sub> and an increase in the amount of CO<sub>2</sub>, with the clear identification of CO (around 6%) (see Fig. 11).

In order to understand the methanation mechanism that explain this process, Gibbs free energy minimization method was employed to predict the distribution of the products in both the solid and gas phase at chemical equilibrium for reaction between MgH<sub>2</sub> and CO<sub>2</sub>. This represents the expected reaction without the use of any catalyst. The mole fraction of the products (%) was obtained as a function of CO<sub>2</sub> pressure at 400°C for a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 4:1 (Fig. 12 A) and 2:1 (Fig. 12B).

From these calculations, it can be inferred that the molar ratio MgH<sub>2</sub>:CO<sub>2</sub> has an influence on the equilibrium composition of the system.

Regarding the gas phase for the relation 4:1, it is expected to be richer in H<sub>2</sub> than in CH<sub>4</sub>, whereas for the relation 2:1 the opposite occurs. In both cases no residual CO<sub>2</sub> or CO formation is expected. For the latter case, the amount of CH<sub>4</sub> produced increases more strongly with pressure. Moreover there are differences in the composition of the solid. While for the relation 4:1 part of the MgH<sub>2</sub> does not react, when the relation 2:1 is considered, only MgO and C are identified as solid products and no MgH<sub>2</sub> is expected. Experimentally, it was determined that the interaction between the CO<sub>2</sub> that reaches the solid surface of the sample and the H<sub>2</sub> released from the hydride depends strongly on the molar ratio between MgH<sub>2</sub> and CO<sub>2</sub>.

Comparing Figure 12 A and B, it is clear that employing a relation 2:1 favors the CH<sub>4</sub> production when no catalyst is added. The experimental results obtained at 400°C (see Table 1) are consistent with the above presented observations. In addition, the same thermodynamic analysis was performed at 450°C (see Fig. S8). Notably, with a 2:1 ratio, if temperature rises from 400 to 450 °C, the amount of CH<sub>4</sub> decreases for a determined pressure, suggesting that this experimental condition is not favorable.

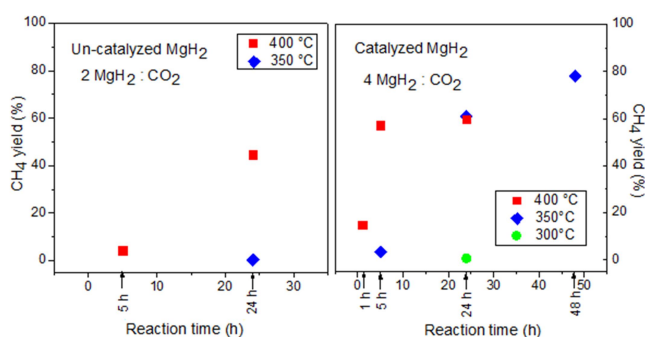


Figure 10: Methane yields (%) obtained after reaction with under CO<sub>2</sub> at different temperatures and reaction times (h).



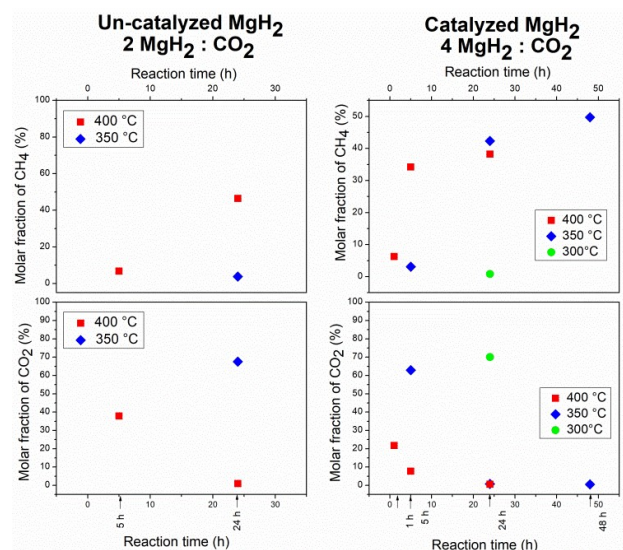


Figure 11: Molar fraction (%) of CH<sub>4</sub> and CO<sub>2</sub> obtained at different temperatures (°C) and reaction times (h) after reaction with CO<sub>2</sub> for the un-catalyzed and catalyzed samples.

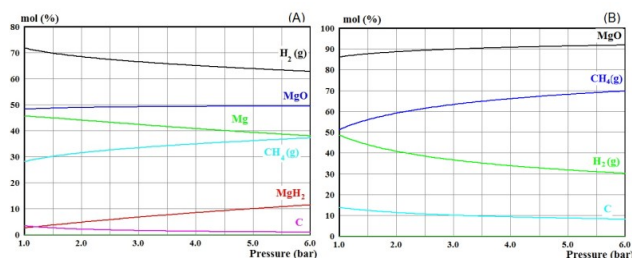
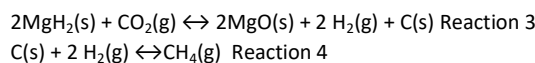


Figure 12: Equilibrium composition (mol%) as a function of pressure at 400 °C for a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 4:1 (A) and 2:1 (B).

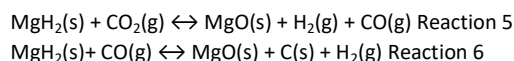
While this seems opposite to previous observations, the kinetics may be favored at higher temperatures.<sup>37</sup> From a thermodynamic point of view, considering a constant pressure of 1 bar, to obtain high CH<sub>4</sub> yield and avoid carbon deposition it is desirable to operate the system at low temperatures (<75°C) because if temperature rises, a mixture of CH<sub>4</sub> and H<sub>2</sub> is obtained (see Fig. S9). However, previous experiments have shown good results exploring the feasibility of conversion at high temperatures (450–500°C).<sup>36–37</sup> Moreover, it was demonstrated that is not possible to lower the reaction temperature without affecting the molar percentage of CH<sub>4</sub> considerably. When the reaction temperature is lowered from 400 to 350°C, the reaction does not progress as expected (see Table 1). The experimental amount obtained of the desired gas product (CH<sub>4</sub>) at 400 °C after treatment of 24 h (46.4 %) was lower than that predicted by the thermodynamic estimations (60%). The difference is attributable to kinetic restrictions and the availability of carbon surface to react with H<sub>2</sub>.

Considering the information presented above, a global mechanism for the direct reduction of CO<sub>2</sub> by MgH<sub>2</sub> without catalyst (also called CO<sub>2</sub> hydrogenation), for a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 2:1, can be

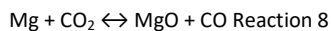
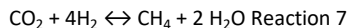
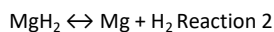
proposed involving reactions 3 and 4. The enthalpy of Reaction 3 is negative in the entire temperature range from ambient onwards and as the temperature rises, it becomes more negative. On the other hand, for Reaction 4, when temperature increases, the enthalpy is less negative and becomes positive for temperatures over 500°C. That is the reason why CH<sub>4</sub> and H<sub>2</sub> always coexist in the gas phase resultant from these samples and it is not possible to obtain pure CH<sub>4</sub>. The thermodynamic calculations predict that reactions 3 and 4 occur simultaneous, changing the relative amounts of coexistent species (C, MgO, CH<sub>4</sub> and H<sub>2</sub>) as a function of pressure.



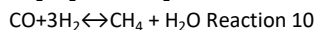
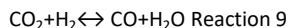
Additionally, when equilibrium is not reached, CO<sub>2</sub> is not totally reduced to C, but it is partially reduced to CO. This explains the presence of CO for short reaction times or low temperatures. In this case, Reaction 5 and Reaction 6 occur in series, with CO as an intermediate in the reduction of CO<sub>2</sub> to carbon. If both reactions are added, the previously proposed Reaction 3 is obtained. Moreover, the detection of small amounts of MgCO<sub>3</sub> can be justified by the magnesium oxide carbonation by reaction with CO<sub>2</sub>, whereas, the generated CO can be consumed to form superior hydrocarbons through a Fischer–Tropsch reaction or other products through different reactions.<sup>46</sup>



The use of catalysts allows the methanation mechanism to be different from the one described above. From Fig. 10 it can be pointed out that, for a 24 h-treatment of the cobalt-catalyzed MgH<sub>2</sub>, it is possible to lower the operational temperature from 400 to 350°C without collapsing the methane yield but a temperature of 300°C is not enough to achieve reasonable conversions. On the other hand, reducing the duration of the reaction to 5h is only feasible at 400°C. The best methane yield (78%) was obtained for the MgH<sub>2</sub>-10 wt% Co sample per treatment under CO<sub>2</sub> for 48 hours at 350°C considering a molar ratio MgH<sub>2</sub>:CO<sub>2</sub> of 4:1 (see Fig. 10). In this condition the gas phase contained 49.7% CH<sub>4</sub> with CO<sub>2</sub> in excess of 0.5% (see Fig. 11). After 24 h of thermal treatment, the gas phase was composed by a mixture of CH<sub>4</sub> (46.4%) and H<sub>2</sub> (52.9%), with a small amount of unreacted CO<sub>2</sub> (0.9%) and practically none CO (<1000 ppm) (see Table 1). The catalyzed process is highly selective to methane, as there was no evidence of the formation of other hydrocarbons such as ethane or propane (see Fig. 7). Then, at 350°C, the longer the time reaction, the more favored the CO<sub>2</sub> conversion is. These observations indicate that even with the use of catalyst, the selection of the appropriate temperature and time reaction is crucial as there is a compromise between these two non-independent parameters. Considering all the experimental evidence, it can be proposed that the process for the MgH<sub>2</sub> catalyzed sample occurs via *Sabatier reaction* according to the global Reaction 7, after MgH<sub>2</sub> decomposition into Mg and H<sub>2</sub> through Reaction 2. This process is favored by active catalysts such as Co. According to the stoichiometry of this reaction, the required molar ratio between MgH<sub>2</sub> and CO<sub>2</sub> is 4:1. Metallic Mg can be oxidized by reaction with CO<sub>2</sub> according to Reaction 8.



The presence of water detected by gas-phase FTIR experiments is strong evidence indicating that the methanation process takes place through the proposed mechanism. Moreover, when the molar ratio  $\text{MgH}_2:\text{CO}_2$  was changed from 4:1 to 2:1, the methanation performance was worsened. CO co-generated could not be avoided and a big amount of  $\text{CO}_2$  remained unreacted (see Table 3). The difference observed respect to the previous results might indicate that the system is disproportioned. Although hydrogen remained in the solid, both in  $\text{MgH}_2$  and  $\text{Mg}_2\text{CoH}_5$ , the amount of  $\text{CO}_2$  is high and limits the release of  $\text{H}_2$  from the hydrides. This limitation may be from a kinetic nature, due to surface passivation as the CO is chemisorbed onto cobalt. Then, unlike what was demonstrated for the un-catalyzed system, in this case the optimal molar ratio is 4:1. These two characteristics confirm that the global process of  $\text{CO}_2$  reduction by catalysed  $\text{MgH}_2$  with Co responds to a *Sabatier process*. It has been previously demonstrated that at 1 bar the  $\text{CH}_4$  selectivity and  $\text{CO}_2$  conversion are optimized at low temperatures and that although the reaction rate increases with temperature, the formation of CO by-product is favored above 450 °C due to reversed water gas shift reaction (Reaction 9).<sup>34</sup> However, depending on the specific catalysis mechanism, the presence of CO can be detected at lower temperatures. CO formation was observed at short reaction times or low temperatures (see Table 3), but, for longer reaction times it is consumed through reaction with  $\text{H}_2$  to generate more  $\text{CH}_4$  (Reaction 10).  $\text{MgH}_2$  was always identified in the solid phase which means that part of  $\text{H}_2$  was retained in the hydride phase, inhibiting to achieve higher conversion rates.



## 5. CONCLUSIONS

In this work, for the first time, the feasibility of the reduction of  $\text{CO}_2$  to  $\text{CH}_4$  using  $\text{MgH}_2$  in the presence and absence of cobalt as catalyst and the most favorable reaction conditions were investigated. It was shown that the methanation mechanism depends on the presence of catalyst and its nature and other factors such as the grade of microstructural refinement, molar ratio  $\text{H}_2:\text{CO}_2$ , reaction time and temperature are crucial and non-independent factors for the process effectiveness. Without catalyst the process is favored employing a molar ratio  $\text{MgH}_2:\text{CO}_2$  of 2:1. In this condition, a methane yield of 44.6% was obtained after 24 h of thermal treatment at 400 °C. As predicted from thermodynamic calculations, the gas phase was a mixture of  $\text{CH}_4$  and  $\text{H}_2$ . The experiments also showed the presence of small amounts of  $\text{CO}_2$ , CO and superior hydrocarbons in the gas phase, whereas the solid product contained Mg, MgO, and C with little  $\text{MgCO}_3$ . The global mechanism for the un-catalyzed  $\text{MgH}_2$  involves the direct reduction of  $\text{CO}_2$  and the generation of  $\text{CH}_4$  via C as an intermediary. When either the temperature or the reaction time is lowered, the performance values drop sharply because while equilibrium is not reached,  $\text{CO}_2$  is not totally reduced to C, but it is partially reduced to CO. Otherwise, for the  $\text{MgH}_2$  catalyzed process the optimal molar ratio was

demonstrated to be 4:1. A methane yield of 78% was achieved by heat treatment at 350 °C for 48 h. The global mechanism responds to a Sabatier process favored by Co as an active catalyst and it also involves reversed water gas shift reaction followed by methanation of CO in presence of steam. The catalyzed process is more selective, as there was no evidence of the formation of superior hydrocarbons.

It was proved that the use of catalyst allows lowering the operational temperature without reducing the methane yield. Then, this investigation provides valuable advances in research related to  $\text{CO}_2$  methanation employing a solid hydrogen storage medium as a  $\text{H}_2$  source.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

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