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Publi	hing ANALYSIS OF SOLAR DIRECT IRRADIANCE MODELS UNDER CLEAR-S	KIES:
2	EVALUATION OF THE IMPROVEMENTS FOR LOCALLY ADAPTED MO	DELS
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18	Abstract	
19		
20	Direct solar irradiance has to be determined for the design of many energy applications	such as PV
21	systems, concentration systems and the generation of solar potential maps for energy use.	Knowledge
22	of the accurate values of radiation components in a local area will allow optimal sizing of s	olar energy
23	conversion systems. Estimated values of direct solar irradiance from models are still n	ecessary at
24	those sites where no measurements are available. In this work, different models used for es	stimation of
25	direct component of solar irradiance are analyzed. Firstly, an evaluation of the performan	ice of eight
26	existing original models was carried out from which three were selected. Secondly, selec	ted models:
27	were calibrated to adapt them to our study geographical area and, which is the important as	spect of this
28	work, an assessment of performance improvements for locally adapted models i	s reported.
29	Experimental data consisted of hourly horizontal global, direct and diffuse solar irradia	nce values,
30	provided by the National Meteorological Agency in Spain (AEMET) for Madrid. Lon,	g-term data
31	series, corresponding to a total period of time of 32 years (1980-2011), have been used in	1 this study.

Publishing clear sky models were treated at the present. The three selected models were adapted to the specific location of Madrid and RMSE and MBE were determined. By comparing the performance in the direct horizontal irradiance estimation from existing original and the corresponding locally adapted models, values of RMSE decreased from 9.9% to 5.7% for the Louche model, from 7.8% to 7.4% for the Robledo-Soler model and finally from 8.8% to 6.7% for the ESRA model. Thus, significant improvements can be reached when parametric models are locally adapted. In our case, it is up to approximately 4% for the Louche model. It is expected that calibrated algorithms presented in this work will be applicable to regions of similar climatic characteristics.

40

41 Keywords: solar radiation, direct irradiance, clearness index, diffuse fraction, Linke turbidity factor

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I. Introduction

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The search for simple, economic energy solutions adapted to local consumption and on a small scale 45 is an emerging need in developed countries [1]. In Spain, as in other European countries, the 46 alternative of "net metering" has been advanced as a solution to the problem of energy supplies [2]. It 47 consists of implementing small installations with mainly renewable energies, which enable self-48 sufficiency of industrial facilities or residential buildings and grid-connected facilities that exchange 49 energy at times of high and low consumption [3]. This solution prevents distribution losses, increases 50 the reserve capacity and promotes the rational distribution of energy. Photovoltaic (PV) and 51 Concentrated Solar Power (CSP) should be seriously considered as technologies that will help to 52 achieve the goal of universal and cheap electricity produced by high-tech devices that collect solar 53 radiation. A more precise knowledge of the solar radiation components in a local area will imply a 54 more optimal design of its solar systems, for example, PV systems use global irradiances while CSP 55 systems use direct irradiance. An accurate prediction of the energy production of a solar system is not 56 57 only vital for its integration in the electric grid but also for the consumer.

58

There are different ways to get the radiation data needed for the calculation of solar facilities such as databases, radiation maps and satellite measurements but, in the majority of cases, these data are not obtained by direct measurement and are not optimal for many localized applications [4]. The models used for the calculation of solar radiation are usually models validated for specific areas and for **P6Blishing** fic geographic and climatic conditions [5]. It is necessary to validate these models and to find adaptations for different conditions and places by adjusting the parameters to the area under study [6].

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Several papers deal with the significance of calculating the incident irradiance components under a 66 cloudless sky. Gueymard [7] pointed to the primordial importance of evaluating the maximum solar 67 68 resource, i.e. the clear-sky direct irradiance, in relation to the use of different energy solar applications particularly those relying on solar concentrators. The importance of clear sky models is mainly 69 because they are a key base for the subsequent application of a cloud factor which leads to irradiance 70 71 under realistic conditions [8]. The significance of solar radiation models in the Heliosat method is of particular interest as the clear-sky model is a key starting point for subsequent cloudy sky models [9, 72 73 10]. In this context, several models have been proposed in the literature [11, 12] so that a previous 74 revision has been carried out in this work.

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Global solar irradiance is more commonly measured at radiometric stations than their components, so 76 77 a number of models were developed to estimate direct or diffuse radiation from the global value. 78 These types of models are called decomposition or separation models [11, 13] as they separate global radiation into its components. Over recent years, a literature search reported 250 such separation 79 methods [11] and different authors have tested the performance of many of these models at different 80 locations and time spans [11, 14-17]. New schemes have recently been proposed [18, 19] to calculate 81 the normal direct irradiance based on the relationship between the diffuse fraction K_d (ratio of diffuse 82 to global irradiance) and the clearness index K_t (ratio of the global irradiance to its corresponding 83 84 extraterrestrial irradiance) in Europe. Factors that influence direct radiation under cloudless skies are atmospheric turbidity, mainly related to the physicochemical properties of aerosols, and precipitable 85 water content [8]; in specific regions, where turbidity and water vapour show little or no fluctuations, 86 solar geometry is the most important factor that models solar irradiance. So, several empirical models 87 88 using solar altitude angle as the only input parameter can be found in the literature [20, 21].

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In this work, eight solar direct irradiance models based on different types of correlations are analyzed. Decomposition models based on the calculation of the diffuse fraction K_d as a function of the clearness index K_t are often used to calculate the direct component [22] and they will be introduced first. Two types of such algorithms, linear and polynomial, can be found in the literature. Here, a

Poblishing sentative linear model due to Reindl [23] and two polynomial models due to Erbs [24] and 95 Muneer [25] have been selected. The Erbs model has been recommended in national standards and 96 included as a reference for the performance assessment [26] and the Muneer model provides a 97 correlation which was fitted to the mean global curve based on curves obtained at worldwide locations 98 [27]. Decomposition models based on diffuse fraction calculations continue to be used [17, 22], 99 mainly due to their simplicity.

100

101 Models with the solar altitude angle, α , as the only input parameter, are very effective when locally 102 adapted coefficients are applied. In this case, the Robledo-Soler model [21] whose authors proposed 103 coefficients for Madrid has been selected.

104

105 The calculation of direct irradiance by using a combination of K_t and α has also been considered. A 106 model also proposed by Reindl et al. [23] which combines both input variables has been included.

107

Models due to Louche et al. [28] and Maxwell [29] have been also selected. These models, widely cited in literature [13, 17, 27], use the clearness index, K_t , to model the atmospheric transmittance rather than the diffuse fraction. They obtain the direct irradiance by multiplying the transmittance by the extraterrestrial irradiance.

112

Finally, the clear sky model used by Ref. [9], the ESRA (European Solar Radiation Atlas) model was selected. The Linke turbidity factor is a key input parameter in this model. For clear days, the Linke factor is, mainly, a function of aerosols and water vapour content. This factor, typically varies from 3 (clear days) to 7 (heavily polluted skies) [30]. Knowledge of this factor in a given location and time is needed for accurate predictions from the ESRA model. Taking this into account, the Linke factor was determined for the location under study.

119

120 The eight studied models are referred in this work as Reindl1 model, Erbs model, Muneer model,
121 Louche model, Reindl2 model, Robledo-Soler model, Maxwell model and ESRA model.

This paper is organized as follows: Climatic conditions and experimental data are described in section
II; the performance of eight clear-sky direct irradiance models is evaluated in section III; this section

- 124 is carried out in three steps: firstly, the selection of clear sky data is described, secondly, the
 - 4

Pl25lishing ematical equations of the eight selected models are shown and thirdly, the performances of the models are analyzed using statistical errors –mean-biased error (MBE) and root mean square error (RMSE). In section IV, three best-performance selected models are calibrated using data from a specific location, Madrid. The improvement of the predictions between parametric models locally adapted with respect to their original formulations is quantified. Final remarks and conclusions are provided in section V.

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II. Climatic conditions and experimental data

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Madrid has a Mediterranean continental climate characteristic of the much of Spain's inland territory, 134 135 where continental features are due to the limited influence of the sea. This type of climate is characterized by wide diurnal and seasonal variations in temperature and by low and irregular rainfall. 136 137 Continental winters are cold and summers are warm and cloudless. Figure 1 shows the annual evolution of mean values of temperature and rainfall at Madrid for the period 1981-2010 138 139 (http://www.aemet.es/es/). Temperature varies from 25.6 °C in July to 6.3 °C in January and rainfall varies from 60 mm in October to 10 mm in August. It is expected that the results from this study will 140 be applicable to regions of similar climatic characteristics [31]. 141



Figure 1. Climatic values (time period 1981-2010) of temperature and rainfall for each month atMadrid (Data obtained from AEMET)



148 Experimental data used in this work consist of measurements of global, diffuse and direct irradiance 149 on a horizontal surface provided by the National Meteorological Agency (AEMET) from the 150 radiometric station sited in Madrid [32]; its geographical coordinates, latitude and longitude, are 40°27' N, 3°43' W at an elevation of 663 meters above sea level. Data on a hourly basis have been 151 managed corresponding to complete years for the period 1980-2011; data from 1980 to 2004 were 152 153 used for model selection and from 2005 to 2011 were used for intercomparisons between original and 154 locally adapted models. Data from 5:00h to 20:00h were available for each day, the irradiance value at 155 a specific time corresponds to an average over the hour before. Time is expressed in True Solar Time (TST). Global and diffuse radiation data were obtained from bimetallic sensors SIAP until 1983, Kipp 156 157 & Zonen CM5 until May 1995, Kipp & Zonen CM11 until December 2004 and Kipp & Zonen CM21 from 2005. Data of direct radiation have been measured by direct sensors Eppley NIP until December 158 2004 and Kipp & Zonen CH-1 from 2005. Diffuse sensors were installed on shadow bands and 159 directly over conventional solar trackers (Eppley) until 2001 and from this date, an automatic solar 160 161 trackers Kipp & Zonen 2AP model has been used. Each sensor is calibrated bi-annually at the National Radiation Centre in Madrid, with reference to a standard pyranometer or pyrheliometer 162 directly referenced to WSG Davos. The AEMET radiometric network has the certification ISO 163 9001:2000. 164

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III. Performance of models

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The objective of this section is to categorize our data into different sky conditions and to evaluate the performance of eight models to calculate clear sky direct horizontal irradiance. A set of 25 years of data corresponding to the period 1980-2004 has been used in this study. The selection of clear sky data is described in subsection III.A. The description of models is made in section III.B and the comparison of models performance is carried out in section III.C.

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175

174 A. Selection of clear sky data

A classification of data into different sky conditions was done previous the application of models. In
order to select clear sky data, different criteria have been proposed in the literature including sky ratio,

Publishing cover, Perez sky clearness index and clearness index between others [27, 33, 34]. We have applied two of them, one is the clearness index, K_t; this index is commonly used due to it is based on the most accessible solar radiation measurement which is horizontal global irradiance [33]. K_t is also used as input parameter in some of the studied models; the other is the more sophisticated Perez clearness index, proposed initially into the Perez model [14] and valued by its high accuracy [33].

183 The Perez sky clearness index,
$$\varepsilon$$
, is defined [14] :

$$\varepsilon = \frac{\frac{D_h + B_n}{D_h} + k\theta^3}{1 + k\theta^3}$$

185 where, D_h is the horizontal diffuse irradiance, B_n , the normal direct irradiance, θ , the solar zenith angle 186 in radians and k, a constant equal to 1.041. Eight categories of cloudiness are defined depending on 187 the value of the ε . Category 1 corresponds to totally overcast and category 8 to totally clear skies. A 188 simplified classification of the values of ε in three categories, overcast, intermediate and clear skies is 189 given in Table I.

190

184

191 **Table I.** Range of values of the Perez sky clearness index ε for three sky conditions, overcast, 192 intermediate and clear sky.

Bin no.	Sky conditions	3
1-2	Overcast skies	1-1.23
3-6	Intermediate skies	1.23-4.5
7-8	Clear skies	4.5-
	Y	

(2)

193 194

195 In this study, a lower limit to select clear-sky data was established at $\varepsilon = 5$ [35], corresponding to 196 category 8 and a part of 7. The clearness index K_t [8] is expressed by:

 $K_t = \frac{G_h}{I_0} \cdot \sin \alpha$

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where G_h is the global horizontal irradiance and I_0 the extraterrestrial irradiance normal to the solar beam defined as $I_0 = I_{sc}E_o$ being I_{sc} , the solar constant and E_0 , the correction factor for the sun-earth distance calculated by [29]:



(4)

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- 204 $E_0 = 1.00011 + 0.034221 \cdot \cos(\Gamma) + 0.001280 \cdot \sin(\Gamma) + 0.000719 \cdot \cos(2 \cdot \Gamma) + 0.000077 \cdot \sin(2 \cdot \Gamma)) (3)$
- 205
- 206 where, Γ , the day angle, is given for each day of the year, J, by:

$$\Gamma = \frac{2 \cdot \pi \cdot J}{365.25}$$

- A lower value of $K_t = 0.6$ to select clear skies [36, 37] has been also tested in the present work as will be described below.
- 210
- 211 In Figure 2, a classification of data based on the Perez index ϵ is shown. Values of global and direct
- horizontal irradiance averaged for each category are presented for a period of 25 years, 1980-2004.
- 213 From this figure, it can be seen, that the proportion of the direct to global horizontal irradiance
- 214 increases when cloudiness decreases, as expected.





217 index ε) at Madrid for the time period 1980-2004.



When the condition $\varepsilon > 5$ is applied, 32% of the whole data are selected as clear-sky data; in case of applying the condition K_t>0.6, 60% of data are selected. It is clear that the first condition is more restrictive. Nevertheless, when applied K_t>0.6 over the selection made based on ε , 1% of data were removed at higher. Thus, 31% of the whole data set was selected as clear sky data and used in this work. As the percentage does not appreciably change, conclusions would be similar if only the criterion based on ε is applied.

225

226 **B. Description of models**

227

With regards to diffuse fraction models, these are based on the relationship K_d - K_t as described in section I; this type of models is still used to estimate horizontal direct irradiance as indicated by recent papers [22, 38]. The clearness index K_t has been already defined by the expression (2); the diffuse fraction is defined as:

(5)

 $K_d = D_h / G_h$

- 232
- 233

where, G_h and D_h are the global and diffuse horizontal irradiances, respectively. K_d - K_t models were initially proposed to calculate diffuse irradiance; however, numerous authors [15, 18, 26] have taken advantage of these models to calculate direct irradiance; Following this idea, in this work, the direct horizontal irradiance B_h is obtained by making the difference between the global and diffuse irradiance, i.e.:

239

$$B_{h} = G_{h} - D_{h} = G_{h} - G_{h}K_{d} = G_{h}(1 - K_{d})$$
(6)

240

For these types of models as well as for the other models selected (described in section I), the mathematical algorithms are given as follows:

244 a) Reindl 1 Model [23]
245
$$B_h = G_h \cdot (1 - K_d)$$

 $K_d = 1.020 - 0.248 \cdot K_t$ $K_t \le 0.30$
246 $K_d = 1.450 - 1.670 \cdot K_t$ $0.30 < K_t < 0.78$
 $K_d = 0.147$ $K_t \ge 0.78$
9

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248	b) Erbs Model [24]	
249		$B_h = G_h \cdot (1 - K_d)$	
	$K_d =$	$1.0 - 0.09K_t$ $K_t \le 0.22$	
250	$K_d =$	$0.9511 - 0.1604 \cdot K_t + 4.388 \cdot {K_t}^2 - 16.638 \cdot {K_t}^3 + 12.336 \cdot {K_t}^4 \qquad 0.22 < K_t \le 0.866 \cdot K_t \le 0.866$	8 (8)
	$K_d =$	0.165 $K_t > 0.8$	
251			
252	c	Muneer Model [25]	
253		$B_h = G_h \cdot (1 - K_d)$	
254	$K_d =$	$+1.006 - 0.317 \cdot K_t + 3.1241 \cdot {K_t}^2 - 12.7616 \cdot {K_t}^3 + 9.7166 \cdot {K_t}^4 $ (9)	
255			
256	d) Louche Model [28]	
257		$B_h = K_b \cdot I_0 \cdot \sin \alpha$	
258		K_b is the atmospheric direct transmittance given by:	
259	$K_b =$	$0.002 - 0.059 \cdot K_t + 0.994 \cdot {K_t}^2 - 5.205 \cdot {K_t}^3 + 15.307 \cdot {K_t}^4 - 10.627 \cdot {K_t}^5$	(10)
260			
261	e	Reindl 2 Model [23]	
262		$B_h = G_h \cdot (1 - K_d)$	
		$K_d = 1.020 - 0.254 \cdot K_t + 0.0123 \cdot \sin \alpha \qquad K_t \le 0.30$	
263		$K_d = 1.400 - 1.749 \cdot K_t + 0.177 \cdot \sin \alpha \qquad 0.30 < K_t < 0.78$	(11)
		$K_d = 0.486 \cdot K_t - 0.182 \cdot \sin \alpha \qquad \qquad K_t \ge 0.78$	
264			
265	f)	Robledo-SolerModel [21]	
266		$B_h = 1201.87 \cdot (\sin \alpha)^{1.346} e^{-0.0041 \cdot \alpha}$	(12)
267			
268	g) Maxwell Model [29]	
269	6	$B_h = I_0 \cdot \sin \alpha \cdot (K_{nc} - (A + B \cdot \exp(m \cdot C)))$	(13)
270	In eq	. (13), the expression between brackets is the direct transmittance, K_n , where:	
271	$K_{nc} =$	$= 0.866 - 0.122 \cdot m + 0.0121 \cdot m^2 - 0.000653 \cdot m^3 + 0.000014 \cdot m^4$	(14)
272	<i>m</i> is t	he relative optical air mass and A, B, C are coefficients which for $K_t > 0.6$ are give	en by:
	10		

$ \Delta $		
Publi	$shing_{5.743} + 21.77 \cdot K_{t} - 27.49 \cdot K_{t}^{2} + 11.56 \cdot K_{t}^{3}$	
273	$B = 41.40 - 118.5 \cdot K_{t} + 66.05 \cdot K_{t}^{2} + 31.90 \cdot K_{t}^{3}$	(15)
	$C = -47.01 + 184.2 \cdot K_t - 222.0 \cdot K_t^2 + 73.81 \cdot K_t^3$	
274		
275	h) Clear-sky ESRA model [9]	
276	A different scheme from those described above is provided by the ES	RA model that refers t
277	atmospheric turbidity parameters to estimate irradiance. This method has be	en evaluated in numerou
278	works [39-41] and shows an acceptable response comparable to that of the n	nost sophisticated model
279	The clear sky ESRA algorithm is given by:	
280		
281	$B_h = I_0 \cdot \sin \alpha \; \exp(-0.8662 \cdot \delta_R \cdot m \cdot T_{Lm2}) \tag{16}$)
282		
283	T_{Lm2} is the Linke turbidity factor for an air mass equal to 2, m is the relative	optical air mass and δ_R
284	the Rayleigh optical depth at air mass m . The exponential part in eq. (16) re	presents the transmittane
285	of the direct radiation under clear skies. All the variation of this transm	nittance with air mass
286	included in the product $m\delta_R(m)$ [9]; T_{Lm2} is a normalized Linke factor independent	endent of the air mass th
287	has been introduced in many European models[41]. δ_R is calculated [42] by t	he expression:
288	$\delta_R = \frac{10}{(6.6296 + 1.7513 \cdot m - 0.1202 \cdot m^2 + 0.0065 \cdot m^3 - 0.00013 \cdot m^4)}$	(17)
289	<i>m</i> is calculated by [42]:	
290	$m = \frac{p}{p_0} \cdot \frac{1}{\sin \alpha + 0.50572 \cdot (\alpha + 6.07995)^{-1.6364}} $ (18)	3)
291	The correction pressure factor is given by:	
292	$\frac{p}{p_0} = \exp(\frac{-z}{8435.2})$ (19)))
293	p_0 is the standard pressure, 1013.25 mb and z=663 m is the height for Madrid	1,
294		
295	C. Comparison of the models	
296		
297	Models described in section III.B were applied to the clear sky data selected	from a period of 25 year
298	(1980-2004). Estimated and measured values of direct horizontal irradiance	e are compared in Figu
299	3(a-h). In the case of the ESRA model, it does not have empirical coe	fficients but its accurate
	11	

Publishing ds on the appropriate knowledge of T_{Lm2} at the site. Values of T_{Lm2} for Madrid were taken from Remund et al. [43] consisting of monthly values generated in the Solar Radiation Data (SODA) project for the period 1981-1990. In graphs of Figure 3, line 1:1 is depicted for each model. The number of pairs of data used in the comparison is 23229. A first impression about models performance can be obtained from these graphs. Thus, the models based on the diffuse fraction, Reindl 1, Reindl 2, Erbs and Muneer underestimate the measured values. In the case of Maxwell model, deviations depend on the value of irradiance; higher errors are expected for higher irradiance values. For the rest of models, lower errors are obtained.





Figure 3. Estimated values of clear-sky direct horizontal irradiance against the corresponding measured values for the eight models analyzed in section III.B for the time period 1980-2004. Solid black line represents the 1:1 relationship.

- Two statistical indicators are used to test the performance of the models [44], the root mean square error (RMSE) and the mean bias error (MBE). These indicators, defined as relative percentages of the mean value, are calculated by the expressions:
- 311



$$RMSE(\%) = \frac{100}{\langle M_i \rangle} \sqrt{\frac{1}{N} \sum_{i=1}^{N} (E_i - M_i)^2}$$

$$MBE(\%) = \frac{100}{\langle M_i \rangle} \frac{1}{N} \sum_{i=1}^{N} (E_i - M_i)$$
(20)

313

312

where, E_i and M_i are the estimated and measured values, respectively, $\langle M_i \rangle$ is the mean value of the measured values, and N is the total number of data in the comparison process.

316

Four ranges of solar altitude angles have been taken to evaluate each model. In Table II, the number of data and the mean value of radiation, obtained from the measured data, in each range are shown as well as the values corresponding to the whole range. In Table III, the values of MBE and RMSE are given for each model and for each solar altitude angles range.

321

Table II. Number of data (N) and mean direct horizontal irradiance from measured data at Madrid for

different solar altitude angle ranges and for the total of data for the period 1980-2004.

α	<20°	20°-40°	40°-60°	>60°	Total
N	1526	8180	8646	4877	23229
Mean B_h (W/m ²)	208.29	416.09	653.97	800.79	571.75

- 324
- 325

326 Table III. Performance of the eight analyzed models in section III.B for different solar altitude angle 327 ranges and the total data based on the time period 1980-2004 at Madrid.

	MBE(%)				RMSE(9	%)			
Model a	<20°	20°-40°	40°-60°	>60°	Total	<20°	20°-40°	40°-60°	>60°	Total
Reindl 1	-19.18	-14.14	-11.06	-9.38	-11.55	22.1	16.2	12.53	10.51	13.23
Erbs	-15.85	-11.3	-8.72	-7.4	-9.17	19.3	13.23	10	8.57	10.71
Muneer	-18.07	-14.45	-12.23	-11.04	-12.59	20.79	15.79	13.1	11.85	13.84
Louche	-11.79	-7.13	-4.37	-2.94	-4.83	16.18	10.32	6.88	5.32	7.54
Robledo-Soler	-0.07	0.48	2.6	1.1	1.55	7.93	7.8	7.68	7.23	7.88
Reindl 2	-13.25	-13.54	-14.91	-15.65	-14.74	17.2	15.73	15.93	16.32	16.79
Maxwell	-1.24	-4.66	-13.32	-22.06	-13.38	7.24	8.66	15.8	23.19	18.91
ESRA	-13.12	-6.59	-1.63	1.25	-2.33	16.15	10.82	7.8	7.48	8.76

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330 RMSE values in Table III show that the best performance models are Maxwell at the solar altitude angles $\alpha < 20^{\circ}$, Robledo-Soler at the range 20°-40° and Louche at $\alpha > 40^{\circ}$. The highest errors may be 331 seen in the Reindl 2 and the Maxwell model; in the case of the Maxwell model, the errors are low for 332 333 low solar altitude angles but increase as this parameter rises; the rest of the models have low errors 334 with RMSE ranging, approximately, between 8 and 14% for the whole data set; slight variations of these numbers can be found within each solar altitude angle range. The lowest RMSE is obtained for 335 336 the Louche model. Regarding to MBE, very small values are obtained in the case of the Robledo-Soler and the ESRA models, indicating no tendency towards under or overestimation. The rest of the 337 338 models have, in most cases, a tendency towards underestimation. As a conclusion, the Louche, the Robledo-Soler and the ESRA models show the best performance. Models based on the K_d - K_t 339 relationship (Reindl 1, Erbs and Munner) have higher errors, although their RMSE values are below 340 14%. 341

342 Table IV shows the performance of the eight models but using data corresponding to the period of years 2005-2011. By comparing Table III and Table IV, some conclusions can be obtained; firstly, it 343 can be seen that the number of years used in the sample affects the results; thus, Table IV shows 344 higher errors due to the smaller data set used in this case of only seven years; however, some models 345 are not so affected as others. Specifically, Robledo-Soler and ESRA model do not significantly 346 modify their total RMSE values when the time period of data changes. Secondly, concerning to the 347 overall models performance, conclusions for Table IV are the same as those described for Table III 348 349 and Louche, Robledo-Soler and ESRA models show also in Table IV the best performance.

- 350
- 351
- Table IV. Performance of the eight analyzed models in section III.B for different solar altitude angle
 ranges and the total data based on the time period 2005-2011 at Madrid.

0.			MBE(%)					RMSE(%)		
Model a	<20°	20°-40°	40°-60°	>60°	Total	<20°	20°-40°	40°-60°	>60°	Total
Reindl 1	-24.09	-20.32	-13.71	-11.54	-15.13	26.16	21.31	14.62	12.32	16.16
Erbs	-20.79	-16.80	-11.08	-9.53	-12.43	23.33	17.92	11.93	10.30	13.44
Muneer	-22.57	-19.62	-14.49	-13.11	-15.69	24.77	20.51	15.12	13.67	16.60

-\											
ubli	shing _{he}	-16.90	-13.09	-6.96	-5.20	-8.37	19.90	14.59	8.39	6.58	9.88
	Robledo-Soler	2.70	-2.47	1.45	-2.68	-1.67	8.11	8.10	7.39	7.30	7.81
	Reindl 2	-18.50	-18.92	-17.03	-17.73	-17.79	21.14	20.10	17.81	18.23	19.32
	Maxwell	-3.11	-9.70	-15.94	-24.39	-16.43	10.01	12.02	17.67	25.24	21.12
	ESRA	-17.29	-8.22	-3.61	-1.12	-4.49	18.99	11.10	7.81	6.87	8.75

- 354
- 355

Our interest in this point is the selection of the models with the best performance. Regarding this, the same conclusions can be obtained from both tables. Thus, those algorithms found to have the best performance (Louche, Robledo-Soler and ESRA) were selected for further analysis that will consist in the obtaining of new models parameters adapted to the studied area.

- 360 361
- IV. Calibration of models
- 362

In order to improve the performance of the models selected in subsection III.C, a local adaptation to a specific site, Madrid, has been carried out. In first place, empirical coefficients were recalculated with data from Madrid for the Louche and the Robledo-Soler algorithms. Regression analyses were performed on algorithms (10) and (12) to obtain new coefficients. Data for the time period 1980-2004 were used in the fitting process. The obtained equations are:

- 368
- 369 Louche model:

370
$$K_b = 1.635 - 4.440 \cdot K_t + 2.455 \cdot {K_t}^2 + 3.876 \cdot {K_t}^3 + 0.646 \cdot {K_t}^4 - 3.673 \cdot {K_t}^5$$
 (21)

(22)

- 371 with $R^2=0.71$
- 372
- 373 Robledo-Soler model:
- 374 $B_h = 1092.475 \cdot (\sin \alpha)^{1.276} \cdot e^{-0.0030 \cdot \alpha}$
- 375 with $R^2 = 0.97$
- 376

377 In the case of Robledo-Soler, their model was originally established for Madrid; therefore, calibrated 378 and original coefficients are close. Nevertheless, greater reliability is achieved here, as the new

Parblishings cients were calculated over a lengthy time span of 25 years while original ones were obtained over a time period of 18 months, June 1994 to November 1995.

381 The treatment in the case of the ESRA model was different. As mentioned above, the accuracy on the 382 outputs from the expression (16) is directly related with the accuracy in T_{Lm2} , therefore, this input

- 383 parameter should be assessed at each site on a climatological basis, season by season [9]. Thus, the
- following part of this section is dedicated to the retrieval of more realistic values of T_{Lm2} for Madrid:
- 385

386 <u>Calculation of the Linke Factor T_{Lm2} for Madrid</u>

387

Values of T_{Lm2} were calculated for Madrid on a hourly basis for the period 1980-2004. This was done through eq. (16) solving for this factor:

390
$$T_{Lm2} = \ln \left(\frac{B_h}{I_0 \cdot \sin \alpha} \right) / (-0.8662 \cdot \delta_R \cdot m)$$
(23)

391

by using the measured direct horizontal irradiance B_h in this period of time as input [39]. Several representative statistical averages for T_{Lm2} were obtained from those hourly values. First, daily values were calculated; these are represented as points in Figure 4. These daily values were used to calibrate the climatological Bourges algorithm [45] that accounts for the annual variation of turbidity [10].

- 396
- 397

$$T_{Lm2} = T_0 + u\cos(\Gamma) + v\sin(\Gamma)$$
(24)

398

399 where, Γ is the day angle redefined using the eq. (4) and T_{0} , u and v are local empirical coefficients to 400 be determined for Madrid. A regression analysis was carried out over the aforementioned data period. 401 The coefficients obtained for Madrid were:

- 402
- 403 404

 $T_0 = 3.25$ u = -0.52 v = -0.06 (25)

with a coefficient of determination of R^2 =0.86. The fitting analysis is graphically shown in Figure 4, where the points represent the averaged measured values of T_{Lm2} for each day number of the year and the line corresponds to the values predicted by the Bourges algorithm.

- 408
- 17





410 411

Figure 4. Daily average values of T_{Lm2} (points on the graph) obtained from experimental data and polynomial regression curve (black solid line) corresponding to estimated values from the Bourges algorithm with coefficients obtained for Madrid for the time period 1980-2004.

415

416 Secondly, monthly mean hourly values of T_{Lm2} were obtained. This type of averaged values has been 417 very useful in different solar radiation studies [46, 47] as they represent typical climatic behavior. These values are shown in Table V. For any month, T_{Lm2} increases as the hour increases, reaching a 418 419 maximum at 12h-13h and then decreases with hours thereafter. Typical behavior is illustrated in Figure 5 which shows the variation of T_{Lm2} with time of day for the month of June. Table V also 420 421 indicates that, at any hour, T_{Lm2} increases with month, reaching a maximum in July and decreases 422 thereafter. Typical behaviour is illustrated in Figure 6 which shows the variation of T_{Lm2} with months of the year at 12h. A variation range for T_{Lm2} between 2.4 and 4 can be established for the overall data. 423 424

425

426 **Table V.** Monthly mean hourly values of the Linke Factor T_{Lm2} at Madrid calculated over the period 427 of time1980-2004 from experimental data of direct horizontal irradiance.



- 432 time 1980-2004
- 433





435

436 Figure 6. Variation of T_{Lm2} with month of year at 12h at Madrid based on the period of time 1980-

437 2004

438

Thirdly, the mean value over the whole set of data was calculated obtaining T_{Lm2} =3.39. The three different statistical averages of T_{Lm2} , i.e., mean daily values, monthly mean hourly values and a constant value of 3.39 have been considered as input in the ESRA model and their respective performances tested over a set of data different from that of the calibration process; this will be discussed in the next section.

444

445 <u>Performance of the calibrated models</u>

446

The performance of equations developed in this section corresponding to calibrated or locally adapted 447 models is next tested. A set of data different from that used in the adaptation process is used. This new 448 449 data set corresponds to the period of years 2005-2011. Based on the same criteria given in the last 450 paragraph of section III.A, 9095 data were selected as clear-sky days. Firstly, the performance of the 451 equations (21) and (22) for the Louche and Robledo-Soler models is analyzed; secondly, the 452 performance of the ESRA model by considering the three different averages for T_{Lm2} described above 453 is tested; here, these approaches will be denominated ESRA 1 (daily T_{Lm2} calculated from Bourges 454 algorithm), ESRA 2 (monthly mean hourly values of T_{Lm2} presented in Table V) and ESRA 3 (a 455 constant value T_{Lm2} =3.39)

P45blishistign ated direct horizontal irradiances from the locally adapted models are compared to measured direct horizontal irradiance in Figure 7. Table VI gives the number of data and mean values for each solar altitude angle range corresponding to the period 2005-2011. In Table VII, the statistical errors MBE and RMSE are given for this validation data set.





Figure 7. Estimated values of clear-sky direct horizontal irradiance against the corresponding measured values for Louche, Robledo-Soler and ESRA locally adapted models. The time period for this performance analysis is 2005-2011. Solid black line represents the 1:1relationship.

461

- 462
- 463 **Table VI.** Number of data (N) and mean direct horizontal irradiance from measured data at Madrid
- 464 for different solar altitude angle ranges and for the total data for the period 2005-2011.

α	<20°	20°-40°	40°-60°	>60°	Total
N	656	3334	3185	1920	9095
Mean B_h (W/m ²)	219.68	430.22	666.96	827.96	581.9

465

466 467

468 Table VII. Performance of the calibrated models (section IV) for different solar altitude angle ranges469 and for the total data based on the time period 2005-2011.

				MBE(%)				RMSE(%)			
Model a	<20°	20°-40°	40°-60°	>60°	Total	<20°	20°-40°	40°-60°	>60°	Total	
Louche	0.42	-4.93	-2.86	-2.42	-3.2	7.96	7.18	5.08	4.74	5.7	
Robledo-Soler	2.4	-2.92	-1.73	-3.3	-2.41	7.44	7.69	6.74	7.02	7.37	
ESRA 1	-2.03	2.08	6.79	7.75	5.56	5.81	6.7	9.25	9.9	9.52	
22											

AIP		This manuscrip	ot was acce	epted by Re	enewable S	Sustainable	Energy. Click	here to see	e the versio	n of record	1.
Publisese	2	-1.12	-1.72	-1.85	-2.2	-1.9	5.12	6.23	6.34	6.59	6.72
ESRA	3	-16.09	-7.8	0.15	3.35	-1.48	17	10.01	6.33	7.05	7.92

470

471

From Table VII, it can be seen that the improvement of the accuracy of models was quite significant; 472 473 the errors diminished with respect to Table IV. Louche, Robledo-Soler and ESRA 2 models perform better than the rest; specifically, total RMSE was reduced from 9.9% to 5.7%, 7.8 to 7.4% and 8.8 to 474 6.7%, respectively. Regarding to the three approaches considered for T_{Lm2} , ESRA 2 approach, which 475 476 considers climatic month-hour values of the Linke factor, gives better estimations than the other two; 477 this is due to ESRA 2 approach considers the significant diurnal variation of the atmospheric turbidity [48] which is larger than the day to day variation (considered in ESRA 1); its MBE and RMSE present 478 similar low values for all the solar altitude angle ranges (MBE=-1.9% and RMSE=6.7% for all data). 479 ESRA 1, which makes use of the Bourges algorithm, also had similar errors for all solar altitude angle 480 ranges (MBE=5.6% and RMSE=9.5% for all data). In the case of ESRA 3, which assume a constant 481 value for T_{Lm2} , the total errors are low (MBE=-1.5% and RMSE=7.9% for all data) but high values are 482 483 found for the range of low solar altitude angles.

The results shown in this section lead to the conclusion that significant improvements can be obtained when applying solar irradiance parametric models adapted to a specific local area. RMSE values diminish around 4% in Louche model and 2% in the ESRA model. In the case of Robledo-Soler model, this value only decrease 0.4% due to their model was originally established for Madrid; calibrated and original coefficients are close which indicates the accurate determination of the original parametric coefficients. The best performance is attributed to Louche model followed by ESRA 2 and Robledo-Soler, with RMSE values of 5.7%, 6.7% and 7.4% respectively.

- 491
- 492 V. Conclusions
- 493

494 Radiation modelling is an important factor in the design of renewable solar power systems. Accurate 495 prediction of the direct component of solar irradiance is essential in applications which require high-496 concentration radiation intensity. To evaluate the performance of solar radiation models, availability 497 of direct irradiance based on long-term experimental data is essential. In the first part of this work, 498 eight well-referenced models were analyzed in order to calculate direct horizontal irradiance under



Pupplishing skies by using experimental data taken in Madrid, Spain, on a hourly basis. The period of time from 1980 to 2004 has been considered for this analysis. Three models with the best performance 500 501 were selected in the next step in order to quantify the improvement in the modelled values by fine-502 tuning them to local conditions. Calibrated algorithms for Madrid are given by the equations (21) and (22) for the Louche and Robledo-Soler models. In the case of ESRA model, three different 503 approaches, regarding to the Linke factor (T_{Lm2}) input values, are considered. Calibrated (locally 504 505 adapted) models were validated against a different set of data corresponding to years 2005-2011. Low performance errors are obtained in general as it is shown in Table VII. When compared with the 506 507 RMSE in Table IV, it can be seen how they have decreased from 9.9 % to 5.7%, 7.8% to 7.4% and 8.8% to 6.7% for the models of Louche, Robledo-Soler and the approach here called ESRA 2, 508 respectively. This means that an improvement up to 4% can be achieved in the direct horizontal 509 irradiance estimations when parametric models are adapted to a specific local site. In the case of 510 511 Robledo-Soler, it is only a 0.4% due to parametric coefficients were also initially established to Madrid. It is expected that calibrated algorithms presented in this work will be useful to estimate solar 512 513 direct horizontal irradiance in regions of similar climatic characteristics.

514

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516

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521 522

523 NOMENCLATURE SECTION

	and the second se	
525	B_n	direct normal irradiance (W/m ²)
526	B _h	direct horizontal irradiance (W/m ²)
527	D_h	diffuse horizontal irradiance (W/m ²)
528	G_h	global horizontal irradiance (W/m ²)
529	E_0	Correction factor for the sun-earth distance

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ΔΙ	Ρ		
Publis	hing	normal extraterrestrial irradiance (W/m ²)	
531	Isc	Solar constant (W/m ²)	
532	J	day number of the year	
533	K_b	atmospheric direct transmittance	
534	K_d	diffuse fraction	
535	K_t	clearness index	
536	MBE	mean bias error (%)	
537	т	relative optical air mass	
538	р	pressure (mb)	
539	p_{0}	standard pressure (1013.25 mb)	
540	RMSE	root mean square error (%)	
541	T_{Lm2}	Linke turbidity factor for an air mass equal to 2	
542	Г	day angle (°)	
543	Ζ	height of the site above sea level (m)	
544	α	solar altitude angle (°)	
545	З	Perez's sky clearness index	
546	δ_R	Rayleigh optical depth	
547	θ	solar zenith angle (°)	
548			
549 550	549 550 References		
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