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# Mechanical Properties of Small Quasi-Square Graphene Nanoflakes

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**Abstract:** The rise of straintronics—the possibility of fine-tuning the electronic properties of nanosystems by applying strain to them—has enhanced the interest in characterizing the mechanical properties of these systems when they are subjected to tensile (or compressive), shear and torsion strains. Four parameters are customarily used to describe the mechanical behavior of a macroscopic solid within the elastic regime: Young’s and shear moduli, the torsion constant and Poisson’s ratio. There are some relations among these quantities valid for elastic continuous isotropic systems that are being used for 2D nanocrystals without taking into account the non-continuous anisotropic nature of these systems. We present in this work computational results on the mechanical properties of six small quasi-square (aspect ratio between 0.9 and 1.1) graphene nanocrystals using the PM7 semiempirical method. We use the results obtained to test the validity of two relations derived for macroscopic homogeneous isotropic systems and sometimes applied to 2D systems. We show they are not suitable for these nanostructures and pinpoint the origin of some discrepancies in the elastic properties and effective thicknesses reported in the literature. In an attempt to recover one of these formulas, we introduce an effective torsional thickness for graphene analogous to the effective bending thickness found in the literature. Our results could be useful for fitting interatomic potentials in molecular mechanics or molecular dynamics models for finite carbon nanostructures, especially near their edges and for twisted systems.



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**Citation:** Serna-Gutiérrez, A.; Cordero, N.A. Mechanical Properties of Small Quasi-Square Graphene Nanoflakes. *Crystals* **2024**, *14*, 314. <https://doi.org/10.3390/cryst14040314>

Academic Editor: Lin Gan

Received: 28 February 2024

Revised: 24 March 2024

Accepted: 27 March 2024

Published: 28 March 2024



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**Keywords:** graphene; mechanical properties; stretching; shear; torsion; straintronics

## 1. Introduction

Strain engineering or “straintronics” has emerged as a way to change the behavior of materials, in particular, 2D nanomaterials, especially graphene [1–9]. In this case, straintronics has been considered in recent years as a way to fine-tune, among other properties, its band gap in order to use it in many different applications [10–19]. In fact, strained graphene nanobubbles have been recently proposed as qubits for quantum computing [20]. It is also possible to take advantage of the changes in properties caused by strain in sensing devices [21]. For instance, a graphene strain sensor that can detect various types of strain induced via stretching, bending and torsion [22] and a graphene-based torsion balance [23] have been constructed. Graphene’s properties make it suitable to be used as an actuator to build artificial muscles [24] and in many other biomedical applications [25].

Material simulation methods can be classified according to, among other criteria, two distinct features. The first one uses classical or quantum mechanics, and the second considers materials as continuous media or takes into account their discrete atomistic nature. Therefore, we can consider four different approaches in the study of carbon nanostructures:

1. Quantum atomistic calculations, which explicitly treat materials as atoms obeying the rules of quantum mechanics. This category includes methods that solve either

- full (like quantum chemistry and Density Functional Theory approaches) or approximate quantum equations (like tight-binding and semiempirical methods). See, for instance, [14,26];
2. Quantum continuous models, in which approximate quantum equation solutions are extrapolated to the continuum limit. See, as an example, [27,28];
  3. Classical atomistic simulations, which consider matter as being built of particles that interact following the equations of classical mechanics with potentials (force fields) that try to mimic experimental properties (or those calculated by quantum methods) using empirical parameters. This category includes static calculations called molecular mechanics (MM), also known as molecular structural mechanics (MSM) or nanoscale continuum modelling (NCM)—in which molecular bonds are considered as springs or beams—as well as classical molecular dynamics (MD). See, for instance, [29,30];
  4. Classical continuous models, traditionally used in engineering. See, as an example, [31,32].

Present computational power precludes using quantum atomistic calculations for very large systems, and multi-scale approaches are employed. In these models, macroscopic parameters for approach 4 are obtained from classical atomistic calculations (approach 3) that, in turn, fit their microscopic parameters using quantum mechanical results (approach 1). Therefore, these multi-scale models need a hierarchy of calculations. Jumping from approach 1 to 3 in the case of deformed graphene is still an open question, and better comprehension of the atomistic mechanisms at work in graphene deformations is needed [33].

There are many studies on the different mechanical properties of both infinite graphene and finite graphene nanostructures [30,34–44]. Nevertheless, there is a lack of a comprehensive study on the three different deformations a graphene nanoflake can be subjected to—stretching, shear and torsion (especially the last one)—and on the validity of the use of macroscopic formulas for isotropic materials [45,46] for this clearly anisotropic system.

We have studied the behavior of six different nearly square graphene nanoflakes of various sizes subjected to the three aforementioned deformations along their two edges (zigzag and armchair) and calculated for each of them Young's and shear moduli and the torsion constant, as well as Poisson's ratio. Our results could be useful for fitting interatomic potentials in MM/MSM/NCM or MD models for finite carbon nanostructures, especially near their edges and for twisted carbon systems. We have also tested how well commonly used formulas for calculating the torsion constant for a thin slab, as well as Poisson's ratio from Young's and shear moduli, perform.

The structure of the paper is as follows. We present in Section 2 (Materials and Methods) first the theoretical model employed, then the systems studied and, finally, the computational method used. Our results are presented in Section 3 in four different subsections: Young's Modulus, Shear Modulus, Torsion Constant and Poisson's Ratio. Finally, the conclusions of the study are summarized in Section 4.

## 2. Materials and Methods

### 2.1. Theoretical Model

Hooke's law states that when a material is loaded within the elastic limit, stress  $T$  is proportional to strain  $q$ :

$$T = -\kappa q. \quad (1)$$

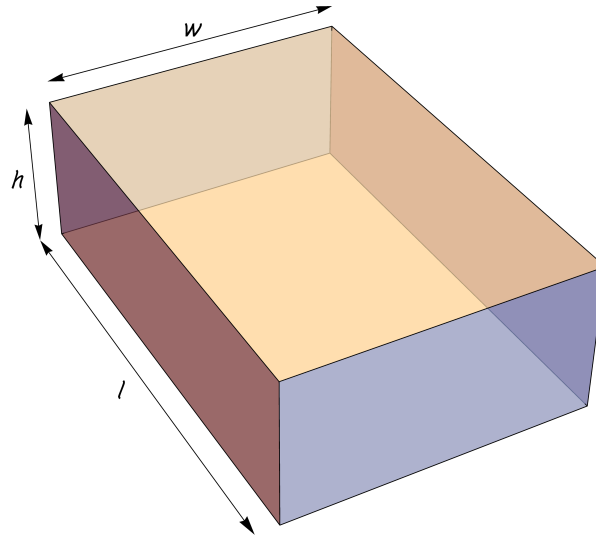
The proportionality constant  $\kappa$  is the so-called elastic constant and can be calculated as the stress/strain ratio associated to a given deformation within the elastic limit.

From a computational point of view, it is easier to adopt a different approach and calculate this constant from the expression for the deformation energy (taking the solid in the absence of any external load as the energy origin) as follows:

$$U = \frac{1}{2} \kappa q^2. \quad (2)$$

Using this energy approach yields values closer to the experimental results than the stress–strain approach since the latter requires an additional process, the differentiation of the energy, which introduces some inaccuracies [47].

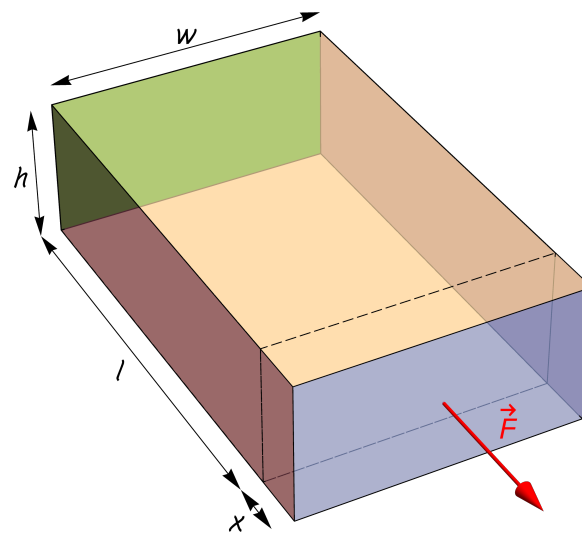
Let us consider the elastic homogeneous and isotropic rectangular parallelepiped solid with length  $l$ , width  $w$  and height  $h$  depicted in Figure 1.



**Figure 1.** An elastic homogeneous and isotropic rectangular parallelepiped solid with length  $l$ , width  $w$  and height  $h$ .

We can load the solid in three different ways in order to obtain three small deformations: stretching, shear and torsion. In the case of uniaxial normal stress (either tensile or compressive), the ratio of the stress (force per unit area) applied to the solid, as depicted in Figure 2 ( $\sigma = \frac{F}{wh}$ ), and the resulting axial strain ( $\varepsilon = \frac{x}{l}$ ) is called the (tensile) elastic modulus or Young's modulus and can be calculated as follows:

$$E = \frac{\sigma}{\varepsilon} = \frac{Fl}{whx}. \quad (3)$$



**Figure 2.** The solid in Figure 1 subjected to a tensile stress caused by fixing the rear face (colored in green) and pulling with a normal force  $\vec{F}$  uniformly distributed over the front face.

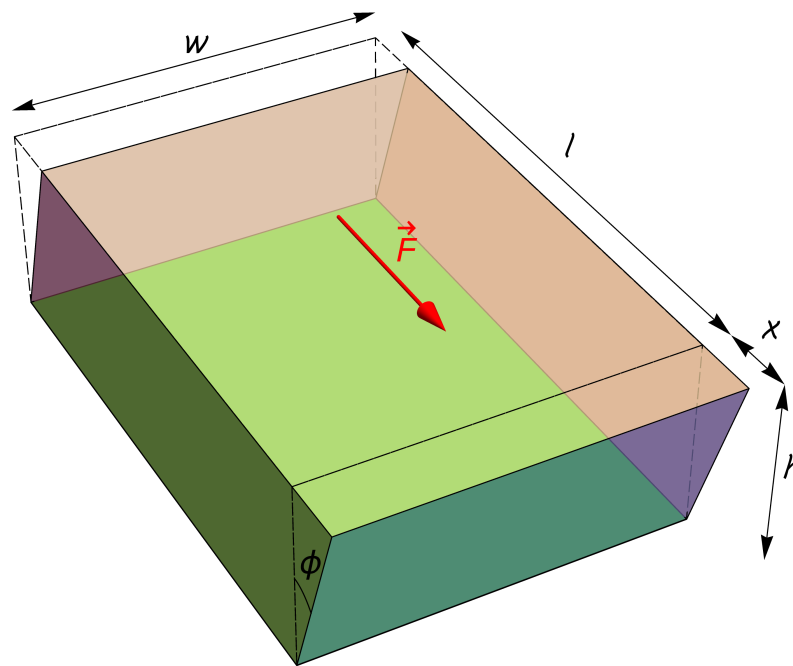
It is easy to prove that the elastic energy of the stretched system is given by using a particular case of Equation (2),

$$U = \frac{1}{2}EV\varepsilon^2, \quad (4)$$

where  $V = whl$  is the volume of the solid.

In the case of uniaxial tangential stress, the ratio of the shear stress (force per unit area) applied to the solid, as depicted in Figure 3 ( $\tau = \frac{F}{wl}$ ), and the resulting shear strain ( $\gamma = \phi \simeq \tan \phi = \frac{x}{h}$ ) is called the rigidity modulus or shear modulus and can be calculated as follows:

$$G = \frac{\tau}{\gamma} \simeq \frac{Fh}{wlx}. \quad (5)$$



**Figure 3.** The solid in Figure 1 subjected to a shear stress caused by fixing the lower face (colored in green) and tearing with a tangential force  $\vec{F}$  uniformly distributed over the upper face.

It is straightforward to prove that the elastic energy of the deformed system is given by using another particular case of Equation (2):

$$U = \frac{1}{2}GV\gamma^2 \simeq \frac{1}{2}GV\phi^2. \quad (6)$$

Finally, in the case of torsion, shown in Figure 4, the ratio of the applied torque  $M$  to the twist angle  $\theta$  is known as torsional stiffness, calculated as follows:

$$k = \frac{M}{\theta}. \quad (7)$$

Once again, it is easy to prove that the elastic energy of the twisted system is given by using a third particular case of Equation (2):

$$U = \frac{1}{2}k\theta^2. \quad (8)$$

Torsion can be seen as a special case of shear, and there exists a relationship between their elastic constants. Taking into account this [48,49],

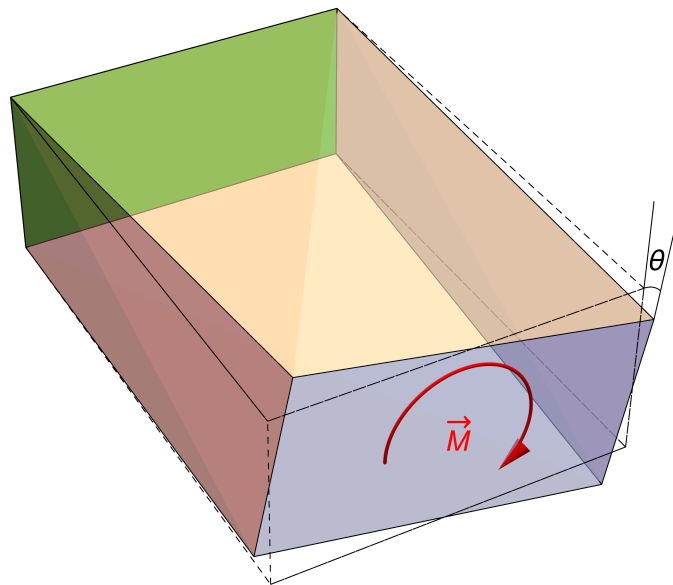
$$\theta = \frac{Ml}{GJ}, \quad (9)$$

where  $J$  is the so-called torsion constant, torsional constant or polar second moment of area (also known as polar moment of inertia). Using this expression and Equation (7),

$$k = \frac{GJ}{l}. \quad (10)$$

$J$  can be calculated by reordering this equation as follows:

$$J = \frac{kl}{G}. \quad (11)$$



**Figure 4.** The solid in Figure 1 subjected to a torsional stress caused by fixing the rear face (colored in green) and twisting with torque  $\vec{M}$  on the front face.

Graphene is considered as a 2D system. It is, in fact, extremely thin, but it has a small thickness due to the electron cloud surrounding the honeycomb structure of carbon nuclei. The accepted value for this thickness is  $3.4 \text{ \AA}$  [50] (though other values are used by different studies, especially in the case of graphene sheets rolled up to build carbon nanotubes [43,51–54]). Therefore, in principle, rectangular graphene nanoflakes could be considered as elastic solids of the type shown in Figure 1 with  $h = 3.4 \text{ \AA}$ . When the thickness of a homogeneous isotropic solid is much smaller than its other two dimensions, there is a formula for calculating the torsion constant [46] that, in our notation, reads:

$$J = \frac{1}{3}h^3w \left[ 1 - \frac{192}{\pi^5} \frac{h}{w} \sum_{n=1,3,5,\dots}^{\infty} \frac{1}{n^5} \tanh \frac{n\pi w}{2h} \right], \quad (12)$$

where, in practice, going up to  $n = 7$  in the series is enough.

Another consideration to take into account is that the situation depicted in Figure 2 is only a first approximation. When a solid is stretched, its perpendicular cross section  $w \times h$  usually changes. In most cases, it decreases. This phenomenon can be measured

by using the so-called Poisson's ratio (denoted by  $\nu$ ), which is the opposite of the ratio of transverse strain to axial strain. For small deformations,  $\nu$  can be calculated as the transversal compression divided by the axial elongation. In our case, for small deformations, the height of the system (i.e., the thickness of the nanoflake) does not change since the breadth of the electron cloud with an appreciable density practically remains constant around the central carbon plane. Therefore,

$$\nu = -\frac{\text{transverse strain}}{\text{axial strain}} = \frac{\text{transverse compression}}{\text{axial elongation}} = -\frac{\Delta w}{x}. \quad (13)$$

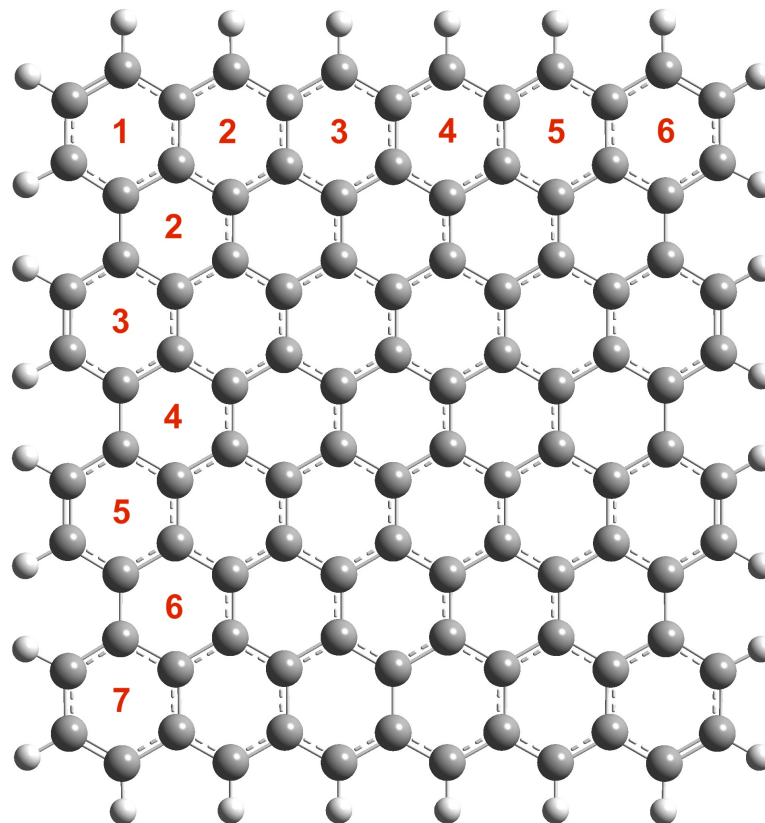
For homogeneous systems, the following expression links Poisson's ratio to Young's and shear moduli:

$$\nu = \frac{E}{2G} - 1. \quad (14)$$

## 2.2. Systems Studied

In order to test whether all the equations valid for homogeneous isotropic systems hold for graphene, which is clearly an anisotropic system, we have selected six small quasi-square hydrogen-passivated carbon nanoflakes. The selection criteria were that the aspect ratio  $\frac{w}{l}$  must lie between 0.9 and 1.1 and that the electronic ground state has to be a spin singlet. The reason for these rules was the need to be able to analyze the effect of the kind of border (zigzag or armchair) without contamination from changes in aspect ratio or spin state. In order to label the nanoflakes, we have used  $n \times m$ , where  $n$  ( $m$ ) is the number of hexagons along the zigzag (armchair) edge. Figure 5 presents as an example the  $6 \times 7$  case, while Figure 6 shows all the nanoflakes studied.

The six stresses considered in this study are shown in Figure 7 for the  $3 \times 3$  nanoflake.



**Figure 5.** A  $6 \times 7$  nanoflake with the hexagons along zigzag and armchair edges numbered.

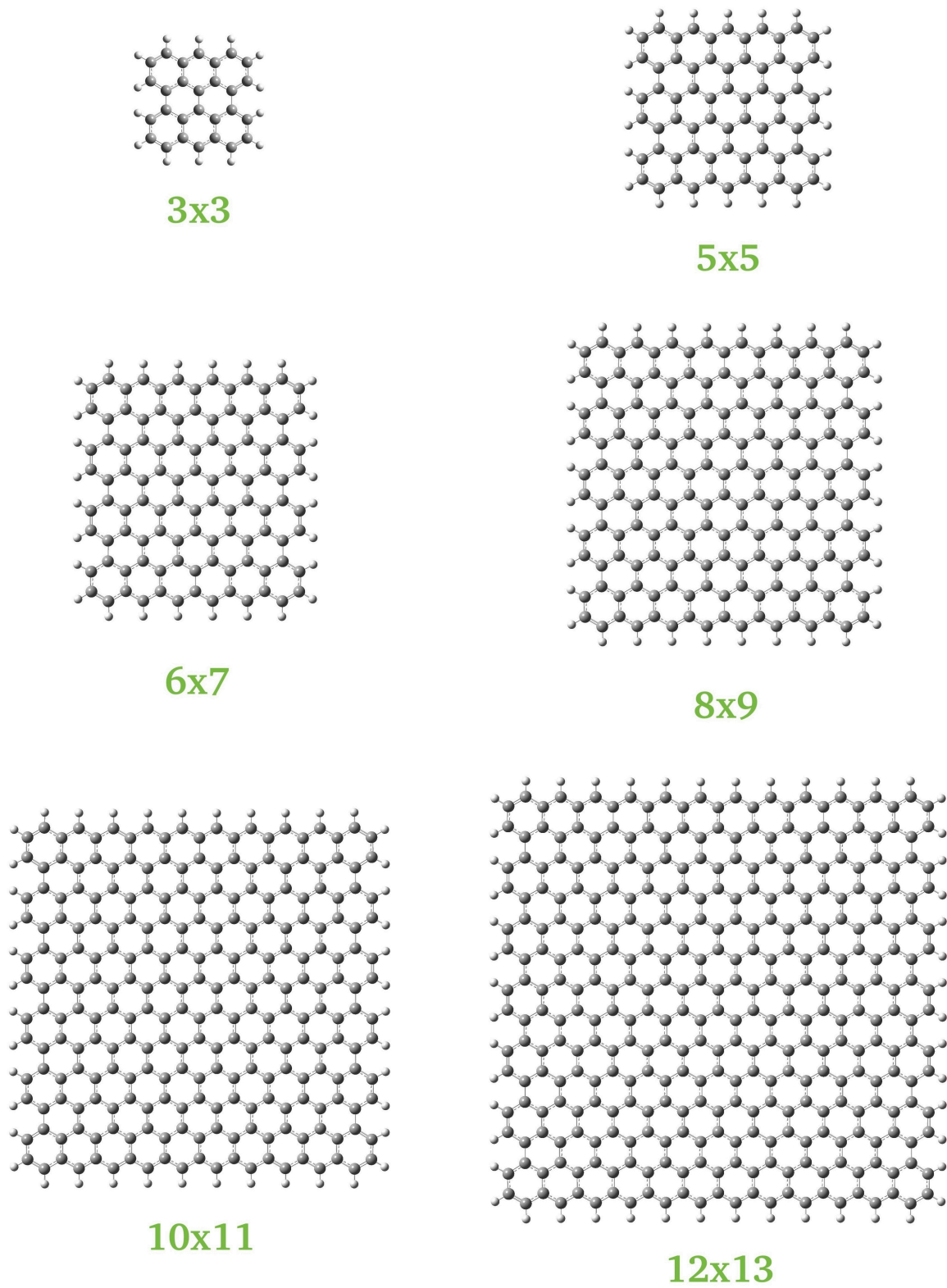
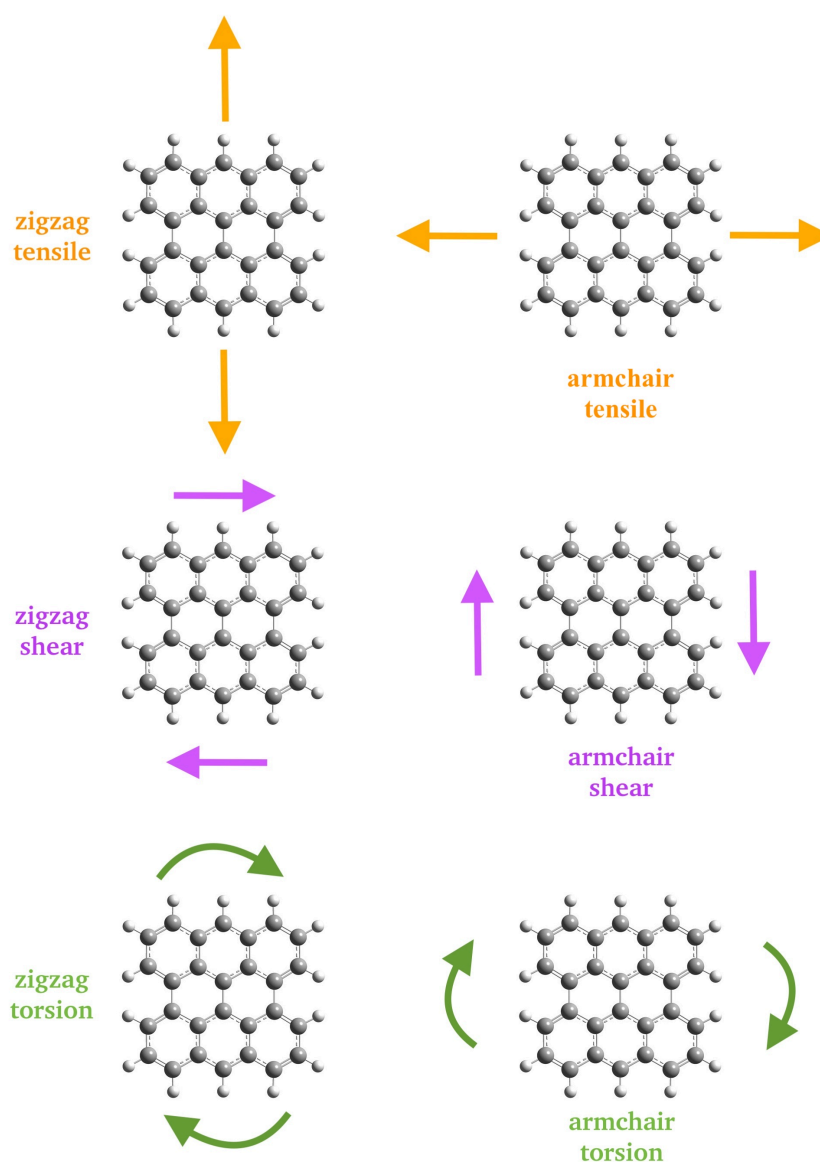


Figure 6. The six nanoflakes considered in this study.



**Figure 7.** The six different stresses considered applied on a  $3 \times 3$  nanoflake: tensile (**top row**), shear (**middle row**), torsion (**bottom row**); zigzag (**left column**), armchair (**right column**).

### 2.3. Computational Method

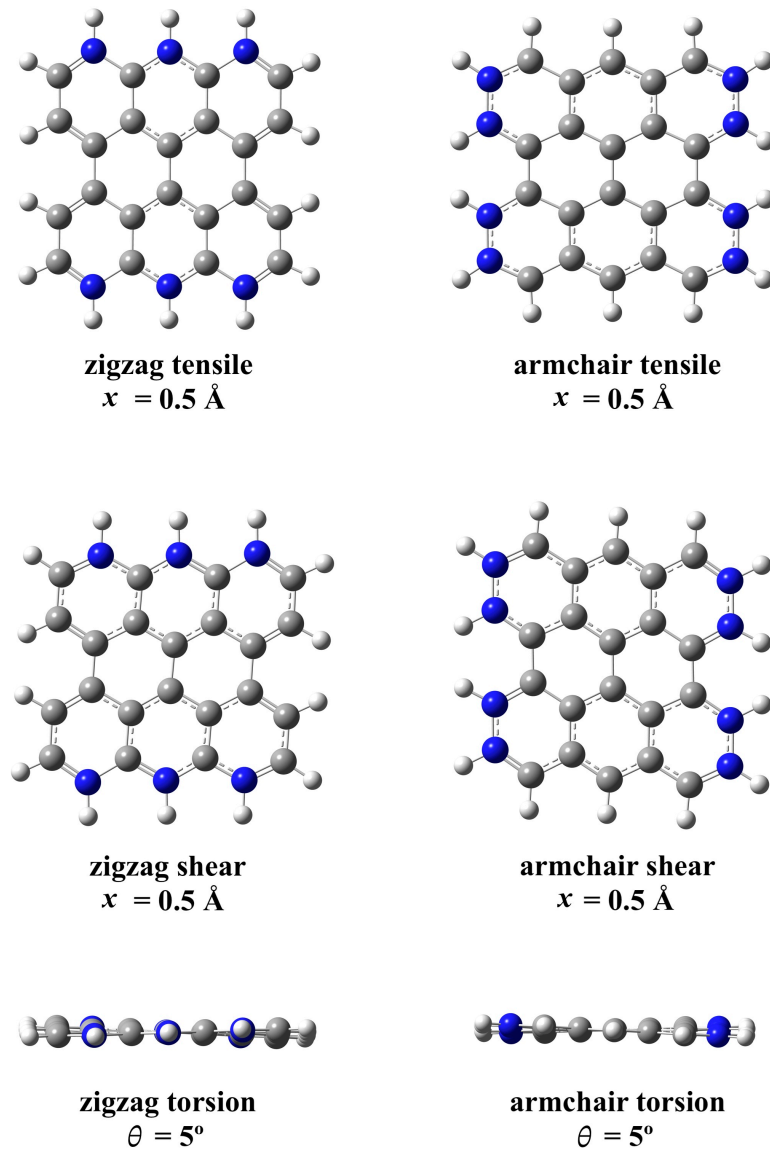
As we pointed out in the Introduction, quantum calculations are needed in order to fit the interatomic potentials used in MM/MSM/NCM and MD methods. Taking into account that these methods only deal with mechanical properties and do not try to explain electronic properties, in order to provide data useful for potential fitting, it is not necessary to use full *ab initio* quantum mechanics calculations (which would be unavoidable when, for instance, establishing the minimum size for antiferromagnetic ordering to appear in finite graphene nanostructures), and semiempirical approaches (much faster than first-principles calculations) are enough for our purpose.

We have selected the semiempirical PM7 method [55], as implemented in Gaussian16 [56] (i.e., PM7R8 [57]), because it is a fast quantum model that explicitly includes dispersion as well as hydrogen bonding corrections and has been successfully used to analyze interactions in graphene nanostructures [58–65].

We have fully relaxed all atomic positions to obtain the different initial geometries. We have calculated all vibrational frequencies to check for the absence of imaginary values



and thus are sure that our initial geometries correspond to minima in the potential energy surface. We have then moved and fixed some boundary atoms in order to deform the nanoflakes and relaxed the positions of the rest of the atoms using the same algorithm to obtain deformation energies. As an example, we present in Figure 8 the final optimized geometries for the six stresses applied to the  $3 \times 3$  nanoflake. The carbon atoms fixed in each case to achieve the desired deformation are highlighted in blue.



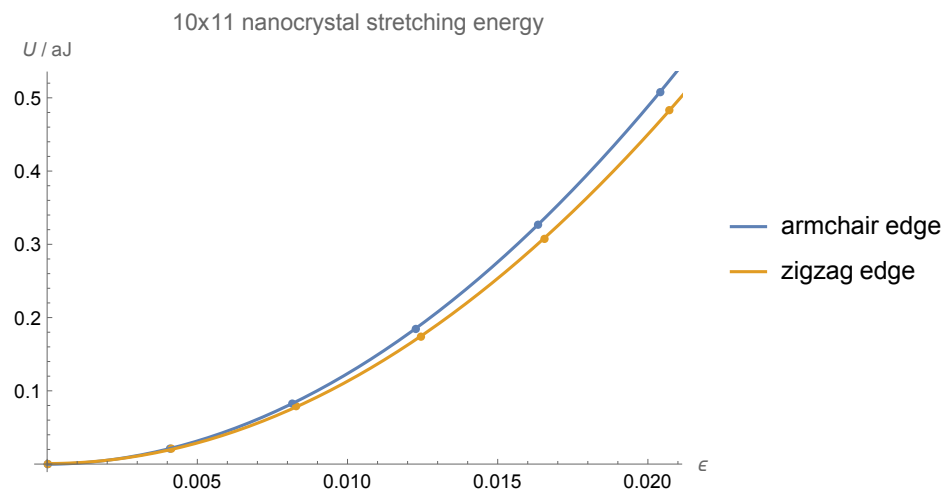
**Figure 8.** The six different optimized geometries corresponding to the maximum deformations applied to the  $3 \times 3$  nanoflake: tensile (**top row**), shear (**middle row**), torsion (**bottom row**); zigzag (**left column**), armchair (**right column**). The carbon atoms fixed to achieve the desired deformation are highlighted in blue.

### 3. Results

#### 3.1. Young's Modulus

We have displaced the carbon atoms on one of the edges along the stretching direction between  $0.1 \text{ \AA}$  and  $0.5 \text{ \AA}$  in  $0.1 \text{ \AA}$  steps, as shown in the upper row of Figure 7, relaxed the rest of the atoms until the new equilibrium geometry depicted in the upper row of Figure 8 is reached and calculated the corresponding strain energies. We have fitted the results to a second-order polynomial and used the quadratic coefficient to calculate  $E$ .

As an example of this procedure, we show in Figure 9 the stretching energies corresponding to both armchair and zigzag edges for the  $10 \times 11$  nanoflake. The graphs for other nanoflakes are similar.



**Figure 9.** Stretching energies  $U$  as a function of strain  $\epsilon$  for the  $10 \times 11$  nanoflake. Points correspond to calculated energies, while lines show a second-order polynomial fit.

We present in Table 1 the geometrical characteristics of the fully relaxed nanoflakes (the lengths of the two carbon atoms' edges and the aspect ratio) as well as our results for their Young's moduli, obtained using Equation (4).

**Table 1.** Young's modulus of square carbon nanoflakes.

Nanoflake	Aspect Ratio	Edge	Edge Length/Å	$E/TPa$
$3 \times 3$	1.03	zigzag	7.099	0.927
		armchair	7.288	1.224
$5 \times 5$	1.07	zigzag	11.368	0.869
		armchair	12.191	1.229
$6 \times 7$	0.94	zigzag	15.618	1.061
		armchair	14.667	1.200
$8 \times 9$	0.98	zigzag	19.879	1.105
		armchair	19.580	1.220
$10 \times 11$	1.01	zigzag	24.143	1.217
		armchair	24.484	1.134
$12 \times 13$	1.04	zigzag	28.388	1.127
		armchair	29.409	1.205

For small nanoflakes, the zigzag results are smaller than the armchair ones, but they increase (while armchair Young's moduli remain practically constant), and both edges show similar  $E$  values, for large nanoflakes. Results from other calculations (in ascending order) are presented in Table 2. It can be seen that our results are in the upper part of the interval defined by all of them, excluding Shi et al.'s value, which is very far from the rest. The table also includes the thicknesses (assumed or calculated) when available.

**Table 2.** Young's moduli ( $E$ ) and thicknesses ( $h$ ) of graphene found in the literature.

Source	$E$ /TPa	Method	$h/\text{Å}$
Reddy et al. [30]	0.671	interatomic potential	3.4
Lebedeva et al. [66]	0.7058–1.343 (depending on the potential used)	interatomic potential	3.34
Giannopoulos [67]	0.745208 for zigzag graphene nanoribbons	spring-based structural mechanics	N/A
Giannopoulos [67]	0.745204 for armchair graphene nanoribbons	spring-based structural mechanics	N/A
Scarpa et al. [68]	0.762–1.000 (depending on the potential used)	cellular material mechanics theory	0.74–0.84
Polyakova et al. [69]	0.820	molecular dynamics	N/A
Tsai and Tu [38]	0.912	molecular dynamics	3.4
Tzeng and Tsai [70]	0.912	molecular dynamics	3.4
Zhang et al. [71]	0.985	spring finite element model	N/A
Sakhaee-Pour [37]	1.040 for zigzag graphene	interatomic potential	3.4
Sakhaee-Pour [37]	1.042 for armchair graphene	interatomic potential	3.4
Sha'bani and Rash-Ahmadi [72]	1.05	molecular dynamics	N/A
Zaeri et al. [73]	1.040	molecular structural mechanics finite element method	3.4
Tapia et al. [74]	1.042	atomistic finite element method	3.4
Anastasi et al. [34]	1.061 for zigzag graphene	molecular dynamics	3.35
Anastasi et al. [34]	1.035 for armchair graphene	molecular dynamics	3.35
Chandra et al. [40]	1.082	atomistic finite element method	1.46
Tahani and Safarian [75]	1.13	homogenization composite shell model	N/A
Cho et al. [35]	1.153 for graphite	molecular mechanics	3.35
Shi et al. [51]	2.81	atomic interaction based continuum model	1.27

The experimental value for the (infinite) graphene Young's modulus is 1.0 TPa [76], very similar to the in-plane Young's modulus in graphite (1.020 TPa [77]). Our results for small nanoflakes are, globally, slightly bigger. This is not surprising since Young's modulus tends to decrease when the size of the system grows from a few tens to a few hundreds of angstroms [78]. The reason is the edge effect on C–C distances. In infinite graphene, all distances are equal. This is not the case for graphene nanoflakes. To show this, we present in Table 3 a comparison between average C–C distances in the central ring (we have selected the nanoflakes with a central hexagon) and on the edge. C–C distances in the center

ring are very close to the experimental infinite graphene value (1.42 Å), but they slightly decrease on the edges. This means C–C bonds are a little bit stronger on the edges of carbon nanoflakes than in graphene, and this translates into an increase in Young’s modulus. As can be seen in the table, the percentage of edge carbon atoms, logically, decreases with the size of the system, but, for our nanoflakes, it is high. For our biggest nanoflake (12 × 13, not shown in the table because it has no central C ring), it is 28%. This explains our values for  $E$  being bigger than that for infinite graphene.

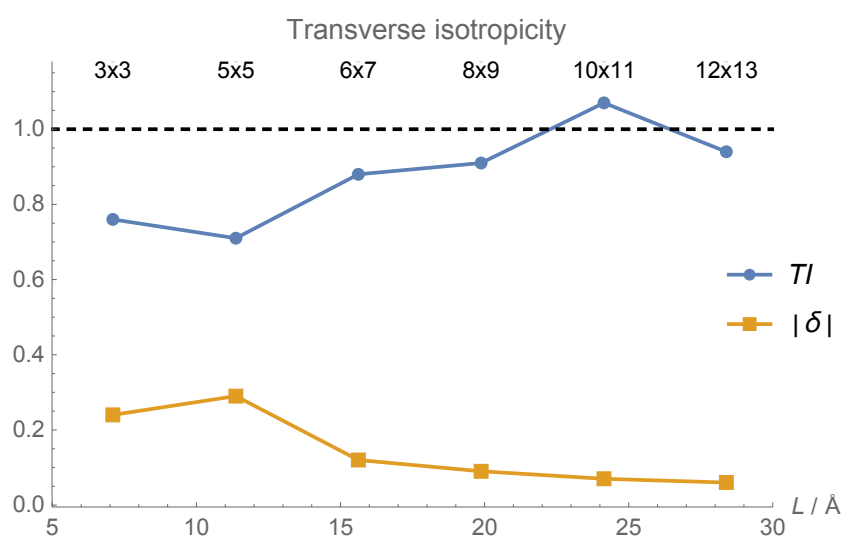
**Table 3.** Average C–C distance in square carbon nanoflakes and percentage of edge C atoms.

Nanoflake	Average C–C Distance		Percentage of Edge C Atoms
	Central Ring	Edge	
5 × 5	1.420	1.399	58 %
6 × 7	1.418	1.402	48 %
10 × 11	1.418	1.403	33 %

As we have pointed out, graphene is clearly an anisotropic system because the properties in the direction perpendicular to the honeycomb plane are completely different to those in plane. Nevertheless, infinite graphene is transversely isotropic, i.e., its properties are symmetric about an axis normal to the honeycomb plane [79]. This means zigzag and armchair Young’s moduli should be equal. In order to test how far our nanoflakes are from this transverse isotropy, we define their transverse isotropy  $TI$  as the ratio of their zigzag and armchair Young’s moduli as follows:

$$TI = \frac{E(\text{zigzag})}{E(\text{armchair})}$$

With this definition, transverse isotropy corresponds to  $TI = 1$ , and anisotropy can be measured as the absolute deviation from this value  $|\delta| = |1 - TI|$ . Using the data in Table 1, we have calculated these two quantities for the six nanoflakes studied. The results are presented in Figure 10. For very small flakes (3 × 3 and 5 × 5), aspect ratio is more important than nanoflake size, and the anisotropy increases with size, but, for the rest of the flakes, as expected, the bigger the flake, the smaller the anisotropy.

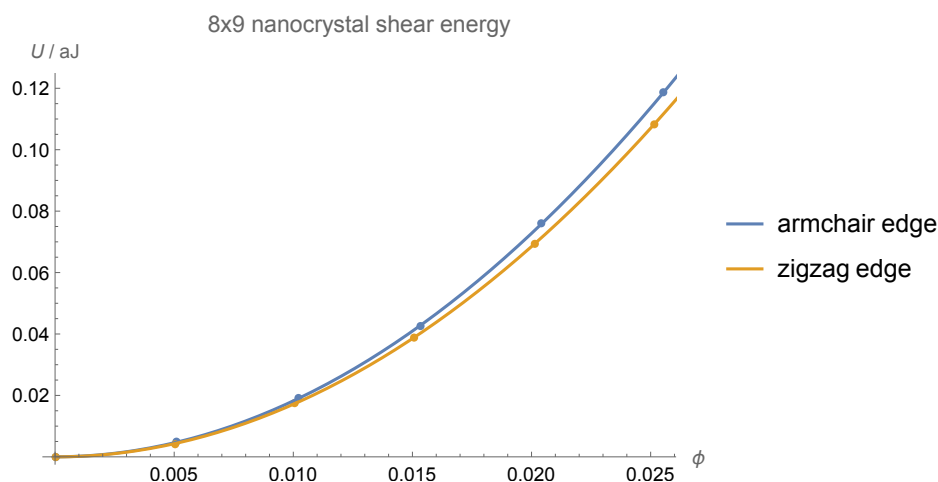


**Figure 10.** Transverse isotropies of the Young’s moduli  $TI$  of the six nanoflakes studied and their anisotropies (absolute deviations from unity)  $|\delta|$  as a function of the zigzag edge length  $L$ .

### 3.2. Shear Modulus

We have displaced the carbon atoms on one of the edges along the shear direction between 0.1 Å and 0.5 Å in 0.1 Å steps, as shown in the middle row of Figure 7, relaxed the rest of the atoms until the new equilibrium geometry depicted in the middle row of Figure 8 is reached and calculated the corresponding strain energies. We have fitted the results to a second-order polynomial and used the quadratic coefficient to calculate  $G$ .

As an example of this procedure, we show in Figure 11 the shear energies corresponding to both armchair and zigzag edges for the  $8 \times 9$  nanoflake. The graphs for other nanoflakes are similar.



**Figure 11.** Shear energies  $U$  as a function of the shear angle  $\phi$  (in radians) for the  $8 \times 9$  nanoflake. Points correspond to calculated energies, while lines show a second-order polynomial fit.

Table 4 presents our results for the shear modulus of the nanoflakes calculated using Equation (6).

**Table 4.** Shear modulus of square carbon nanoflakes.

Nanoflake	Edge	$G$ /GPa
$3 \times 3$	zigzag	221
	armchair	255
$5 \times 5$	zigzag	226
	armchair	259
$6 \times 7$	zigzag	189
	armchair	288
$8 \times 9$	zigzag	263
	armchair	279
$10 \times 11$	zigzag	222
	armchair	240
$12 \times 13$	zigzag	229
	armchair	250

Armchair values for  $G$  are bigger than zigzag ones, in agreement with Sakhae-Pour [37] and Min and Aluru [36].

Results from other calculations (in ascending order) are presented in Table 5. Our results agree very well with most of them and are similar to the experimental value for graphene, which is 280 GPa [80]. It is worth noting that the shear modulus for graphite is 440 GPa [77]. This is proof of the fact that using in-plane graphite properties for isolated graphene is not always valid.

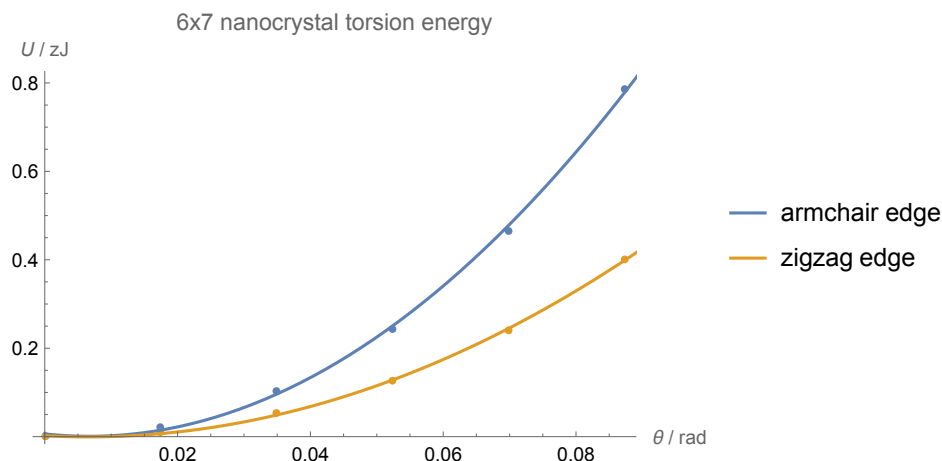
**Table 5.** Shear moduli ( $G$ ) and thicknesses ( $h$ ) of graphene found in the literature.

Source	$G$ /GPa	Method	$h/\text{Å}$
Mukhopadhyay et al. [81]	125.4	molecular mechanics	3.4
Scarpa et al. [68]	202–270 (depending on the potential used)	cellular material mechanics theory	0.74–0.84
Tahani and Safarian [75]	212	homogenization composite shell model	N/A
Sakhaee-Pour [37]	213 for zigzag graphene	interatomic potential	3.4
Sakhaee-Pour [37]	228 for armchair graphene	interatomic potential	3.4
Tapia et al. [74]	213	atomistic finite element method	3.4
Zhang et al. [71]	242	spring-based finite element model	N/A
Georgantzinis et al. [82]	280	spring-based finite element model	3.4
Polyakova et al. [69]	302	molecular dynamics	N/A
Reddy et al. [30]	384	interatomic potential	3.4
Tsai and Tu [38]	358	molecular dynamics	3.4
Zheng et al. [83]	434	beam finite element method	3.4
Zakharchenko et al. [39]	445	atomistic Monte Carlo based on empirical bond order potential	N/A
Min and Aluru [36]	$\approx 460$ for zigzag graphene	molecular dynamics	3.335
Min and Aluru [36]	$\approx 360$ for armchair graphene	molecular dynamics	3.335
Cho et al. [35]	482 for graphite	molecular mechanics	3.35
Zaeri et al. [73]	490	molecular structural mechanics finite element method	3.4
Chandra et al. [40]	606	atomistic finite element method	1.46

### 3.3. Torsion Constant

We present in Table 6 our results for the torsion constant of the nanoflakes calculated using Equations (11) and (12). In the first case, we have twisted one of the edges between  $1^\circ$  and  $5^\circ$  in  $1^\circ$  steps, as shown in the lower row of Figure 7, relaxed the rest of the atoms until the new equilibrium geometry depicted in the lower row of Figure 8 is reached and calculated the corresponding strain energies. We have fitted the results to a second-order polynomial and used the quadratic coefficient to calculate the torsional stiffness according to Equation (8). We have then used our values for  $G$  and  $l$  and employed Equation (11) to determine  $J$ .

As an example of this procedure, we show in Figure 12 the torsion energies corresponding to both armchair and zigzag edges for the  $6 \times 7$  nanoflake. The graphs for other nanoflakes are similar.



**Figure 12.** Torsion energies  $U$  as a function of the torsion angle  $\theta$  for the  $6 \times 7$  nanoflake. Points correspond to calculated energies, while lines show a second-order polynomial fit.

**Table 6.** Torsion constant and effective torsional thickness of square carbon nanoflakes.

Nanoflake	Edge	$J/(10^{-40} \text{ m}^4)$		$\tilde{h}/\text{\AA}$
		Equation (11)	Equation (12)	
$3 \times 3$	zigzag	3.89	64.9	0.71
	armchair	7.02	62.6	0.98
$5 \times 5$	zigzag	10.0	126	0.88
	armchair	6.76	116	0.75
$6 \times 7$	zigzag	10.1	157	0.80
	armchair	12.2	169	0.85
$8 \times 9$	zigzag	7.08	219	0.58
	armchair	12.6	223	0.76
$10 \times 11$	zigzag	16.6	280	0.79
	armchair	22.2	276	0.92
$12 \times 13$	zigzag	28.7	342	0.94
	armchair	30.1	329	0.99

The first thing to notice is that the direct use of Equation (12) with the standard value for graphene thickness  $h$  is not valid. This expression for homogeneous isotropic systems overestimates the value of  $J$  by an order of magnitude. The situation is similar to what happens for graphene bending rigidity  $B$ . Using continuous mechanics expressions for thin plates leads to a value for  $B$  one order of magnitude larger than  $B$  values obtained based on atomic-level calculations [84–87]. In fact, as we have already pointed out, there are several proposals for graphene thickness, and some of them arise precisely from trying to apply equations valid for homogeneous isotropic solids to 2D systems. Values of  $h$  determined from calculations on bent graphene sheets and carbon nanotubes (which can be seen as a particular case of bent carbon nanoribbons) are very different from the standard value  $h = 3.4 \text{ \AA}$  used in stretched (or compressed) planar graphene (the so-called “Yakobson’s paradox”). Using molecular mechanics calculations, Duan et al. reported  $0.52 \text{ \AA}$  [88], Scarpa et al.  $0.84\text{--}1 \text{ \AA}$  [68] and Shi et al.  $1.27 \text{ \AA}$  [51], while Yakobson et al. obtained  $0.66 \text{ \AA}$  using molecular dynamics simulations [29]. From ab initio calculations, Kudin et al. [89] obtained  $0.894 \text{ \AA}$ , Wang et al.  $0.665 \text{ \AA}$  [90] and Shenderova et al.  $0.9 \text{ \AA}$  [91]. Following this idea of an effective bending thickness, we report in the last column of the table the effective torsional thickness  $\tilde{h}$  defined as the value of  $h$  that has to be used in Equation (12) in order to obtain the same value for  $J$  as the one obtained directly from torsion data and Equation (11). Our values for the effective torsional thicknesses are similar

to these effective bending thicknesses and compatible with the upper limit for the effective single-walled carbon nanotube thickness determined by Pine et al.,  $h \leq 1 \text{ \AA}$  [92].

Focusing on the results obtained using Equation 11, with the exception of in the  $5 \times 5$  case, the torsion constant is greater when the nanoflake is twisted around the armchair edge, and, globally,  $J$  increases with the size of the system. Both behaviors are in agreement with results obtained in previous studies [93–95]. In this case, we cannot compare our numerical results to those in the literature because we have found neither calculations nor experiments dealing with any of our nanoflakes, and neither torsional stiffness nor torsion constant are intrinsic material properties but depend on the exact geometry of the system. Results for twisting are by far less abundant than those for other deformations, and our results could be useful for fitting interatomic potentials (especially for torsion and out-of-plane  $sp^2$  hybridization terms in MM/MSM/NCM and MD models) for finite carbon nanostructures.

### 3.4. Poisson's Ratio

Table 7 includes our results for the Poisson's ratio of the nanoflakes calculated using Equations (13) and (14). In the first case, we have used the optimized stretched geometries obtained for determining Young's moduli, measured the transverse compression at the center of the nanoflake and computed  $\nu$ .

**Table 7.** Poisson's ratio of square carbon nanoflakes.

Nanoflake	Edge	$\nu$	
		Equation (13)	Equation (14)
$3 \times 3$	zigzag	0.33	1.09
	armchair	0.43	1.40
$5 \times 5$	zigzag	0.30	0.93
	armchair	0.39	1.38
$6 \times 7$	zigzag	0.33	1.81
	armchair	0.35	1.09
$8 \times 9$	zigzag	0.31	1.10
	armchair	0.34	1.19
$10 \times 11$	zigzag	0.31	1.74
	armchair	0.36	1.36
$12 \times 13$	zigzag	0.31	1.46
	armchair	0.33	1.41

It is clear that Equation (14) overestimates the value of  $\nu$  and cannot be used for these systems. This fact has been previously found for boron nitride nanoflakes [96,97], which also have a honeycomb structure. Results obtained by applying the definition of Poisson's ratio given by Equation (13) indicate that  $\nu$  is bigger for stretching and pulling on the armchair edges (in agreement with Sakhaee-Pour [37]) but that the difference decreases as the size of the nanoflakes increases.

Results from other calculations are presented (in ascending order) in Table 8. We do not include thicknesses in this case because  $h$  is not needed in order to calculate  $\nu$ . Poisson's ratio is strongly dependent on the strain applied (it can even become negative for large strains) [98,99]. In the table, we have selected the values corresponding to the smallest strain possible, but not all cases correspond to the so-called zero-strain limit. That is the reason for the variety of results reported, except for in the last case; Sakhaee-Pour's results [37] are much higher than those from other calculations because he uses Equation (14) to determine  $\nu$ .



**Table 8.** Poisson's ratios ( $\nu$ ) of graphene found in the literature.

Source	$\nu$	Method
Tapia et al. [74]	0.072	atomistic finite element method
Zakharchenko et al. [39]	$0.16 \pm 0.03$	atomistic Monte Carlo based on empirical bond order potential
Shodja et al. [47]	0.19–0.20	Density Functional Theory
Cho et al. [35]	0.195 for graphite	molecular mechanics
Scarpa et al. [68]	0.211–0.848 (depending on the potential used)	cellular material mechanics theory
Lebedeva et al. [66]	0.221–0.987 (depending on the potential used)	interatomic potential
Tsai and Tu [38]	0.26	molecular dynamics
Caillerie et al. [100]	0.26	interatomic potential
Huang et al. [33]	0.28–0.30	bond-orbital tight-binding
Jiang et al. [98]	0.3	molecular mechanics
Cadelano et al. [101]	0.31	tight-binding
Tahani and Safarian [75]	0.333	homogenization composite shell model
Wang et al. [99]	0.35	molecular dynamics
Polyakova et al. [69]	0.36	molecular dynamics
Zhang et al. [71]	0.366	spring-based finite element model
Huang and Hwang [54]	0.397	interatomic potential
Lu and Huang [102]	0.398	molecular mechanics
Reddy et al. [30]	0.428	interatomic potential
Zheng et al. [83]	0.46	beam finite element method
Koberidze [103]	0.51	density-functional tight-binding
Georgantzinis et al. [82]	0.603	spring-based finite element model
Chandra et al. [40]	0.62	atomistic finite element method
Sakhaee-Pour [37]	1.285 for zigzag graphene *	interatomic potential
Sakhaee-Pour [37]	1.441 for armchair graphene *	interatomic potential

\* taking into account that his naming convention is the opposite to ours.

Our results should be compared to those from Jiang et al. [98] and Wang et al. [99], which correspond to the zero-strain limit. The agreement with those results is complete. Regarding experiments, the experimental value of  $\nu$  for graphite is 0.160 [77] and, for graphene, 0.19 [104], but those papers do not indicate the strain, and it is not possible to know how far they are from the zero-strain limit.

#### 4. Conclusions

We have studied the mechanical properties of six small nearly square graphene nanoflakes using the semiempirical PM7 model. We have considered stretching, shear and torsion deformations along zigzag and armchair edges, calculating Young's and shear

moduli as well as the torsion constant and Poisson's ratio. Results obtained could be useful for fitting interatomic potentials (especially for torsion and out-of-plane  $sp^2$  hybridization terms and for near-the-edge bonds in MM/MSM/NCM and MD models) for finite carbon nanostructures. Our results are close to other calculations and to experimental values corresponding to infinite graphene, when these are available. Additionally, by making use of these results, we have tested two formulas valid for macroscopic homogeneous isotropic systems that are sometimes used for 2D nanostructures. We have shown that they do not hold for graphene and explained some strange results reported in the literature. In an attempt to recover one of these formulas, we have introduced an effective torsional thickness for 2D crystals analogous to the effective bending thickness found in the literature. The fast methodology developed in this work can be extended to two other dimensional nanostructures—fully planar and buckled—providing valuable results in order to fit interatomic potentials for faster and more reliable molecular mechanics and molecular dynamics calculations in these systems.

**Author Contributions:** Conceptualization, N.A.C.; methodology, N.A.C.; software, A.S.-G. and N.A.C.; validation, A.S.-G. and N.A.C.; formal analysis, A.S.-G. and N.A.C.; investigation, A.S.-G.; writing—original draft preparation, N.A.C.; writing—review and editing, A.S.-G. and N.A.C.; visualization, A.S.-G. and N.A.C. All authors have read and agreed to the published version of the manuscript.

**Funding:** This work was supported by the European Union NextGenerationEU (PRTR C17.I1).

**Institutional Review Board Statement:** Not applicable.

**Informed Consent Statement:** Not applicable.

**Data Availability Statement:** The original contributions presented in the study are included in the article, further inquiries can be directed to the corresponding author.

**Conflicts of Interest:** The authors declare no conflicts of interest. The funders had no role in the design of the study; in the collection, analyses or interpretation of data; in the writing of the manuscript; or in the decision to publish the results.

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